STORMWATER MANAGEMENT REPORT

Triangle Farm Mill Street Holliston, Massachusetts

June 15, 2020

Prepared for:

Murch Prentice Realty Trust 5855 Lyman Road Turin, NY 13473

Prepared by:

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6-15-2020

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Project Introduction:

The applicant, Murch Prentice Realty Trust, is proposing to develop a seven (7) lot single family Open Space Residential Subdivision located off Mill Street in Holliston, Massachusetts. The existing property consist of approximately 12.4 acres of land area, with additional land area to be considered Open Space.

The Project will be serviced by town water, onsite sewage disposal systems and other available public utilities. The stormwater generated from the Project will be captured, conveyed, treated and mitigated on-site utilizing Best Management Practices.

The purpose of these calculations is to demonstrate design compliance of the Project's stormwater management system for water quality and quantity, specifically post-development peak discharge rates per the DEP's Stormwater Management Policy, the Town of Holliston Land Subdivision Regulations. As designed, the system will mitigate peak rates of runoff for storms up to and including the 100-year event under post-construction conditions.

Methodology/Sources of Data:

The overall storm water management plan for the project is designed to maintain the peak rate of storm water runoff and runoff volumes from the site after development. The Soil Conservation Service Modified Soil Cover Complex Method, the computer program "HydroCAD" by Applied Microcomputer Systems, and the procedures specified in Urban Hydrology for storm Small Watersheds were used to determine pre-and post-developed peak flow rates of runoff from the site. The storm events have been compiled from the Soil Conservation Services Technical Report No. 55 and the U.S. Department of Commerce Technical Paper (TP 40). The 2-year, 10-year, 25-year and 100-year storm events have been utilized for hydrology calculations. The rainfall data for the Type III, 24-hour storm events follow:

24-Hour Storm	Rainfall (inches)
2	3.20
10	4.80
25	5.50
100	7.0

The storm water runoff will be controlled through the use of "Best Management Practices" and in conformance with the MADEP Stormwater Management Policy. The proposed Project will result in an improvement over the existing conditions, by constructing a storm water management system that will provide treatment, groundwater recharge and reduce the peak rates of runoff and offsite runoff volumes.

The piped drainage system has been designed utilizing the Rational Method for the 25 year storm event to size street drains.

Soils:

The Natural Resources Conservation Service (NRCS), Hydrologic Soils Group Map for Middlesex county, Massachusetts indicates that the on-site soils consist of Paxton Fine Sandy Loam-307B, and Scituate fine sandy loam-315B. NRCS assigned hydrologic soil rating for these soils ranges from C and D soil classification. The upper regions of the site consists of C hydrologic soil rating and D rating in the wetland area. On-site soil testing was performed to determine groundwater elevations and confirm soil classifications.

Existing Conditions Overview:

The Project is located off Mill Street and identified as Assessor Map 7, Block 4, Lot 55.2 containing approximately 12.4 +/- acres. The site is currently undeveloped historical farm lands that has become overgrown with brush and woods mix. There is a bordering vegetated wetland area located at the rear of property. The site gently slopes from Mill Street (North) to the rear property boundary (South) with a change in elevation of approximately fourteen (14) feet.

The existing site is divided into three (3) existing watershed subcatchment areas. See the attached Pre-Development Subcatchment Area Plan for delineations. Subcatchment E1 flows overland towards Mill Street and the wetland area to the south. Subcatchments E1 and E2 are combined with Link 1L and discharge via overland flow the rear wetland area.

<u>Description</u>	Design Point Comments
E1	Overland flow to Mill Street area
E2	Overland flow to the rear wetland
E3	Overland flow to the rear wetland

Proposed Conditions Overview:

The proposal is to subdivide the property as an Open Space Residential Subdivision consisting of seven (7) single family dwellings. The proposed roadway extends from Mill Street to a cul-de-sac approximately five-hundred (500) feet in length. The proposed stormwater drainage system is designed to capture the runoff utilizing catch basins, manholes and culverts to convey the stormwater to a drainage basin located at the end of the proposed roadway. The roof runoff from the proposed dwellings will be conveyed via gutters and downspouts to underground recharge systems.

The proposed runoff areas have been divided into four (4) subcatchments. Subcatchment P1 discharges via overland flow towards Mill Street and the wetland area to the south. Subcatchments P3 and P4 bypass the proposed drainage basin and discharge via overland flow to the rear wetland. Subcatchment P4 is directed to the proposed stormwater drainage basin. The outflow from the drainage basin has been combined with the discharge from P3 and P4 in Link 2L for comparison with predeveloped flows.

The proposed systems will reduce all post-development flow rates and volumes of runoff up to and including the 100-year event to existing levels at all abutting areas. Existing uncaptured off-site runoff not associated with the Project will continue to flow overland without change.

<u>Description</u>	Design Point Comments
P1	Overland flow to Mill Street area
P2	Overland flow to the rear wetland
P3	Overland flow to the rear wetland
P4	To drainage basin

The following is summary comparison of Pre- and Post-Developed Rates and Volumes of Runoff:

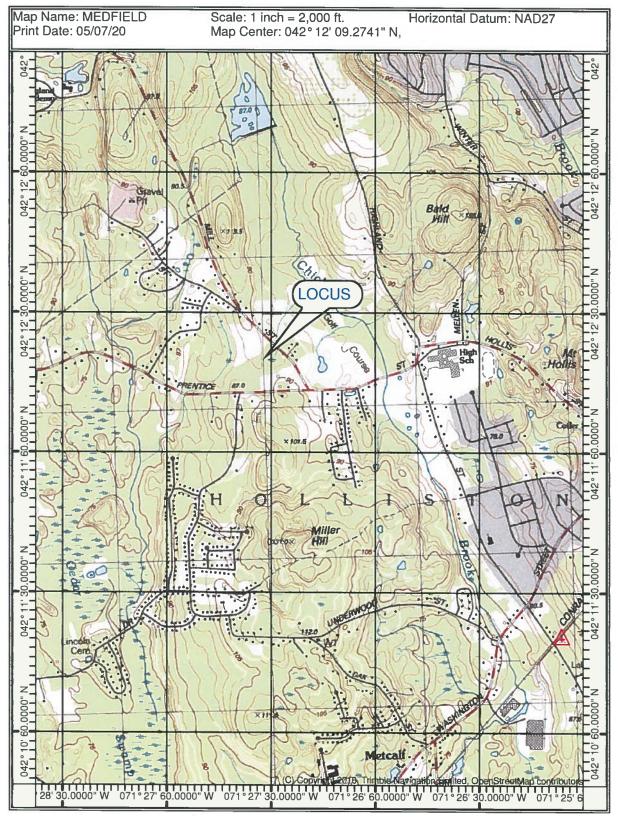
	Summary of Peak Stormwater Runoff Rates:								
Design		ak Flow	10-Yr Peak Flow		25-Yr Peak Flow		100-Yr Peak Flow		
Point	<u>(c</u>	<u>fs)</u>	<u>(c</u>	(cfs)		<u>(cfs)</u>		<u>(cfs)</u>	
	<u>Existing</u>	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed	
E1/	2.59	2.58	5.94	5.63	6.62	6.25	11.15	10.29	
P1									
1L/	4.52	3.64	10.67	9.09	11.93	10.31	20.34	18.31	
2L									

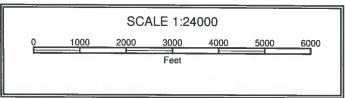
The following is a summary of the Retention Basin:

Summary of Retention Basin								
<u>Design Point</u>	ign Point 2-Yr Volume 10-Yr Volume 25-Yr Volume 100-Yr Volume					Volume		
	(cu.ft.)		(ac-ft) (ac		c-ft)	(a	c-ft)	
	<u>Peak</u>	Outflow	Peak	Outflow	<u>Peak</u>	Outflow	<u>Peak</u>	Outflow
	Elev.Ft.	(cfs)	Elev. Ft.	(cfs)	Elev.Ft.	(cfs)	Elev.Ft.	(cfs)
1P	280.73	0.65	281.43	2.20	281.53	2.54	282.06	4.61

Summary:

The calculations performed for all design storm events indicate that the total peak rates and volumes of runoff for the Project as proposed will not exceed those of existing conditions with the implementation of the stormwater management system. With the implementation of the stormwater management system as designed, along with the Operation and Maintenance plan contained herein, all of the objectives of the DEP's Stormwater Management Regulations are satisfied.





Natural Resources Conservation Service

Web Soil Survey National Cooperative Soil Survey

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MAP LEGEND

C C/D D Not rated or not available satures Streams and Canals rtation Rails Interstate Highways	US Routes Major Roads Local Roads
C/D C/D Water Features Water Features Transportation H++ Rai	Background
Area of Interest (AOI) Soils Soil Rating Polygons A/D A/D B/D B/D C C C C C C C C C C C C C C C C C C C	C/D D Not rated or not available Soil Rating Lines

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25,000.

Warning: Soil Map may not be valid at this scale.

line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause

Please rely on the bar scale on each map sheet for map measurements. Natural Resources Conservation Service Web Soil Survey URL: Source of Map:

Coordinate System: Web Mercator (EPSG:3857)

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

Aerial Photography

B/D

8

8

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Middlesex County, Massachusetts Survey Area Data: Version 19, Sep 12, 2019

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jul 28, 2019—Aug

Not rated or not available

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Soil Rating Points

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8

B/D

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
33B	Raypol silt loam, 0 to 5 percent slopes	B/D	3.8	1.0%
44A	Birdsall mucky silt loam, 0 to 1 percent slopes	C/D	19.1	4.9%
51A	Swansea muck, 0 to 1 percent slopes	B/D	11.8	3.0%
52A	Freetown muck, 0 to 1 percent slopes	B/D	25.2	6.4%
71B	Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony	D	9.9	2.5%
73B	Whitman fine sandy loam, 0 to 3 percent slopes, extremely stony	D	24.1	6.1%
103C	Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes	В	0.2	0.0%
104C	Hollis-Rock outcrop- Charlton complex, 0 to 15 percent slopes	D	4.0	1.0%
106C	Narragansett-Hollis- Rock outcrop complex, 3 to 15 percent slopes	A	25.7	6.5%
251B	Haven silt loam, 3 to 8 percent slopes	А	24.8	6.3%
253C	Hinckley loamy sand, 8 to 15 percent slopes	Α	0.1	0.0%
253D	Hinckley loamy sand, 15 to 25 percent slopes	A	4.8	1.2%
254B	Merrimac fine sandy loam, 3 to 8 percent slopes	A	21.6	5.5%
255B	Windsor loamy sand, 3 to 8 percent slopes	A	23.2	5.9%
261A	Tisbury silt loam, 0 to 3 percent slopes	С	16.8	4.3%
302B	Montauk fine sandy loam, 0 to 8 percent slopes, extremely stony	С	6.1	1.5%

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
302C	Montauk fine sandy loam, 8 to 15 percent slopes, extremely stony	С	5.2	1.3%
307B	Paxton fine sandy loam, 0 to 8 percent slopes, extremely stony	С	23.2	5.9%
307C	Paxton fine sandy loam, 8 to 15 percent slopes, extremely stony	С	5.7	1.5%
315B	Scituate fine sandy loam, 3 to 8 percent slopes	D	41.2	10.4%
317B	Scituate fine sandy loam, 3 to 8 percent slopes, extremely stony	D	35.8	9.1%
335B	Rainbow silt loam, 3 to 8 percent slopes	C/D	0.2	0.1%
336B	Rainbow silt loam, 3 to 8 percent slopes, very stony	C/D	5.0	1.3%
340B	Broadbrook very fine sandy loam, 3 to 8 percent slopes	D	1.1	0.3%
341B	Broadbrook very fine sandy loam, 3 to 8 percent slopes, very stony	D	12.8	3.2%
341C	Broadbrook very fine sandy loam, 8 to 15 percent slopes, very stony	D	0.8	0.2%
424B	Canton fine sandy loam, 3 to 8 percent slopes, extremely bouldery	A	19.5	4.9%
424C	Canton fine sandy loam, 8 to 15 percent slopes, extremely bouldery	А	16.9	4.3%
424D	Canton fine sandy loam, 15 to 25 percent slopes, extremely bouldery	A	5.6	1.4%
Totals for Area of Inter	rest		394.2	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher





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Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.





A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



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Checklist for Stormwater Report

B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature

77777	PHONE STERED TO THE ENGINEER	Filmy 6-19-2020	
L		Signature and Date	

Checklist Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment? New development Redevelopment Mix of New Development and Redevelopment



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Checklist for Stormwater Report

Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

\boxtimes	No disturbance to any Wetland Resource Areas
\boxtimes	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	Credit 1
	Credit 2
	☐ Credit 3
	Use of "country drainage" versus curb and gutter conveyance and pipe
	Bioretention Cells (includes Rain Gardens)
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
	Other (describe):
Sta	ndard 1: No New Untreated Discharges
\boxtimes	No new untreated discharges
\boxtimes	Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
\boxtimes	Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



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Checklist for Stormwater Report

Checklist (continued) Standard 2: Peak Rate Attenuation Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding. Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm. Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm. Standard 3: Recharge Soil Analysis provided. Required Recharge Volume calculation provided. Required Recharge volume reduced through use of the LID site Design Credits. Sizing the infiltration, BMPs is based on the following method: Check the method used. Static
 St Dynamic Field¹ Runoff from all impervious areas at the site discharging to the infiltration BMP. Runoff from all impervious areas at the site is not discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume. Recharge BMPs have been sized to infiltrate the Required Recharge Volume. Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum extent practicable for the following reason: Site is comprised solely of C and D soils and/or bedrock at the land surface M.G.L. c. 21E sites pursuant to 310 CMR 40.0000 ☐ Solid Waste Landfill pursuant to 310 CMR 19.000 Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable. ☐ Calculations showing that the infiltration BMPs will drain in 72 hours are provided. Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



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Checklist for Stormwater Report

Checklist (continued) Standard 3: Recharge (continued) The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided. Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas. Standard 4: Water Quality The Long-Term Pollution Prevention Plan typically includes the following: Good housekeeping practices; Provisions for storing materials and waste products inside or under cover; Vehicle washing controls: Requirements for routine inspections and maintenance of stormwater BMPs; Spill prevention and response plans; Provisions for maintenance of lawns, gardens, and other landscaped areas; Requirements for storage and use of fertilizers, herbicides, and pesticides; Pet waste management provisions; Provisions for operation and management of septic systems: Provisions for solid waste management; Snow disposal and plowing plans relative to Wetland Resource Areas; Winter Road Salt and/or Sand Use and Storage restrictions; Street sweeping schedules; Provisions for prevention of illicit discharges to the stormwater management system; Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL; Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan; List of Emergency contacts for implementing Long-Term Pollution Prevention Plan. A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent. Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge: is within the Zone II or Interim Wellhead Protection Area is near or to other critical areas is within soils with a rapid infiltration rate (greater than 2.4 inches per hour) involves runoff from land uses with higher potential pollutant loads. ☐ The Required Water Quality Volume is reduced through use of the LID site Design Credits.

☑ Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if

applicable, the 44% TSS removal pretreatment requirement, are provided.



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Checklist for Stormwater Report

CI	necklist (continued)
Sta	indard 4: Water Quality (continued)
\boxtimes	The BMP is sized (and calculations provided) based on:
	☐ The ½" or 1" Water Quality Volume or
	☐ The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
	The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
	A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Sta	ndard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
	The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior to</i> the discharge of stormwater to the post-construction stormwater BMPs.
	The NPDES Multi-Sector General Permit does <i>not</i> cover the land use.
	LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
	All exposure has been eliminated.
	All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
	The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.
Sta	ndard 6: Critical Areas
	The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
	Critical areas and BMPs are identified in the Stormwater Report.



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Checklist for Stormwater Report

Checklist (continued)

Sta ext	ent The	rd 7: Redevelopments and Other Projects Subject to the Standards only to the maximum practicable project is subject to the Stormwater Management Standards only to the maximum Extent cticable as a:
		Limited Project Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area. Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
		Bike Path and/or Foot Path Redevelopment Project Redevelopment portion of mix of new and redevelopment.
	The implied the and	tain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an elanation of why these standards are not met is contained in the Stormwater Report. Project involves redevelopment and a description of all measures that have been taken to prove existing conditions is provided in the Stormwater Report. The redevelopment checklist found follows 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment of Structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) proves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



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Checklist for Stormwater Report

Checklist (continued) Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued) ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has not been included in the Stormwater Report but will be submitted before land disturbance begins. ☐ The project is *not* covered by a NPDES Construction General Permit. ☐ The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report. The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins. Standard 9: Operation and Maintenance Plan The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information: Name of the stormwater management system owners; Party responsible for operation and maintenance; Schedule for implementation of routine and non-routine maintenance tasks; Plan showing the location of all stormwater BMPs maintenance access areas; Description and delineation of public safety features; Estimated operation and maintenance budget; and Operation and Maintenance Log Form. The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions: A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs; A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions. Standard 10: Prohibition of Illicit Discharges The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges: An Illicit Discharge Compliance Statement is attached;

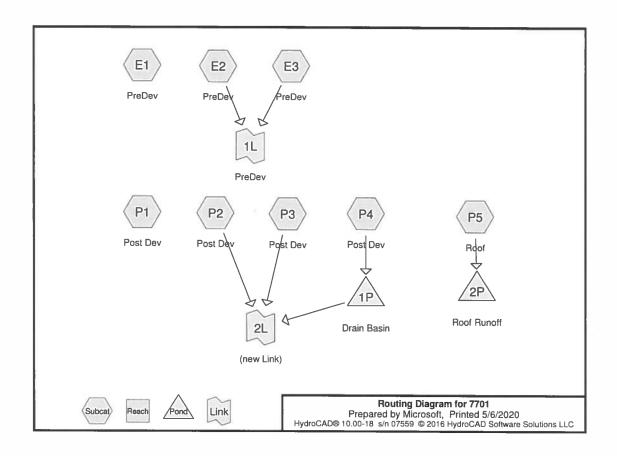
NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of

any stormwater to post-construction BMPs.

APPENDIX - A

Hydrogeological Calculations for Pre & Post Development Hydraulic Design (Manning's Equation)

Standard 2



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Type III 24-hr 2 Yr Rainfall=3.20" Printed 5/6/2020 Page 2

Summary for Subcatchment E1: PreDev

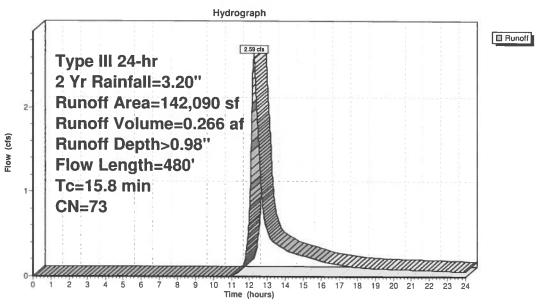
Runoff = 2.59 cfs @ 12.24 hrs, Volume=

0.266 af, Depth> 0.98"

Aı	rea (sf)	CN [Description					
5,670 98 Paved parking, HSG C								
1	36,420	72 \	Voods/gra	ss comb., G	Good, HSG C			
1	42,090	73 \	Veighted A	verage				
1	36,420			vious Area				
	5,670	3	3.99% Impe	ervious Area	a a constant of the constant o			
Tc (min)_	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
13.5	50	0.0160	0.06		Sheet Flow, A-B			
0.6	130	0.0500	3.60		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps			
1.7	300	0.0200	2.87		Shallow Concentrated Flow, C-D Paved Kv= 20.3 fps			
15.8	480	Total						

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Subcatchment E1: PreDev



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Summary for Subcatchment E2: PreDev

Runoff = 3.29 cfs @ 12.25 hrs, Volume=

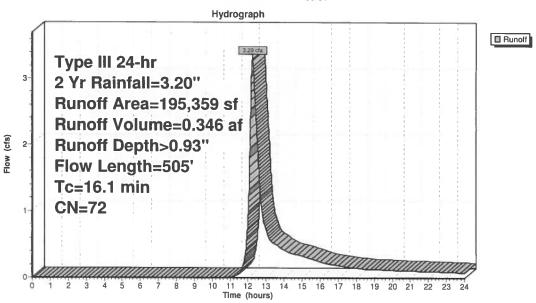
0.346 af, Depth> 0.93"

Α	rea (sf)	CN I	Description				
195,359 72 Woods/grass comb., Good, HSG C							
1	195,359	1	00.00% Pe	ervious Are	a		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
13.2	50	0.0170	0.06		Sheet Flow, A-B		
2.2	270	0.0160	2.04		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps		
0.7	185	0.0800	4.55		Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps		
 16.1	505	Total					

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Subcatchment E2: PreDev



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Type III 24-hr 2 Yr Rainfall=3.20"
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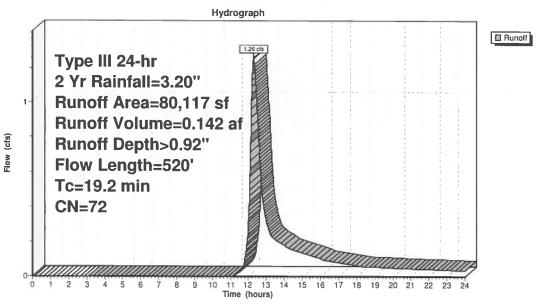
Summary for Subcatchment E3: PreDev

Runoff = 1.26 cfs @ 12.29 hrs, Volume=

0.142 af, Depth> 0.92"

Α	rea (sf)	CN D	escription				
80,117 72 Woods/grass comb., Good, HSG C							
_	80,117	1	00.00% P	ervious Are	ea		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)			
16.3	50	0.0100	0.05		Sheet Flow, A-B		
2.9	470	0.0280	2.69		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps		
19.2	520	Total					

Subcatchment E3: PreDev



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Summary for Subcatchment P1: Post Dev

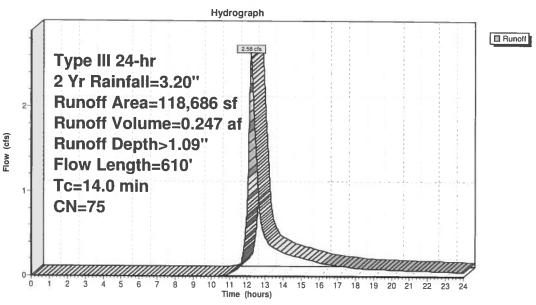
Runoff =

2.58 cfs @ 12.21 hrs, Volume=

0.247 af, Depth> 1.09"

	Α	rea (sf)	CN	Description		
		0	98			
		8,060	98	Paved park	ing, HSG C	
		51,270				ood, HSG C
		59,356	72	Woods/gra	ss comb., C	Good, HSG C
	1	18,686	75	Weighted A	verage	
	1	10,626		93.21% Pe	rvious Area	
		8,060		6.79% Imp	ervious Are	a
	Tc	Length	Slope			Description
_	(min)	(feet)	(ft/ft)		(cfs)	
	10.8	50	0.0100	0.08		Sheet Flow, A-B
						Grass: Dense n= 0.240 P2= 3.20"
	0.6	110	0.0400	3.22		Shallow Concentrated Flow, B-C
						Unpaved Kv= 16.1 fps
	2.6	450	0.0200	2.87		Shallow Concentrated Flow, C-D
_						Paved Kv= 20.3 fps
	14.0	610	Total			

Subcatchment P1: Post Dev



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Summary for Subcatchment P2: Post Dev

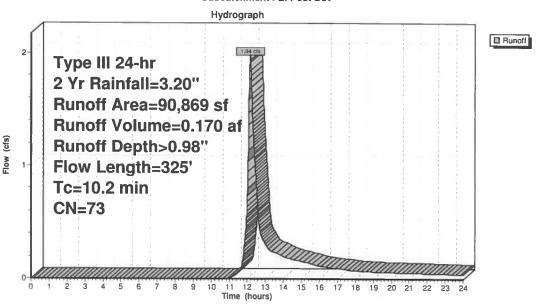
Runoff = 1.94 cfs @ 12.15 hrs, Volume=

0.170 af, Depth> 0.98"

	Α	rea (sf)	ÇN	Description	ı	
		43,772	72	Woods/gra	ss comb., C	Good, HSG C
_		47,097	74	>75% Gras	s cover, Go	od, HSG C
		90,869 90,869	73	Weighted A 100.00% P	Average ervious Are	a
_	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
	9.2	50	0.015	0.09		Sheet Flow, A-B
_	1.0	275	0.080	4.55		Grass: Dense n= 0.240 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	10.2	325	Total			

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Subcatchment P2: Post Dev



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Type III 24-hr 2 Yr Rainfall=3.20" Printed 5/6/2020 Page 12

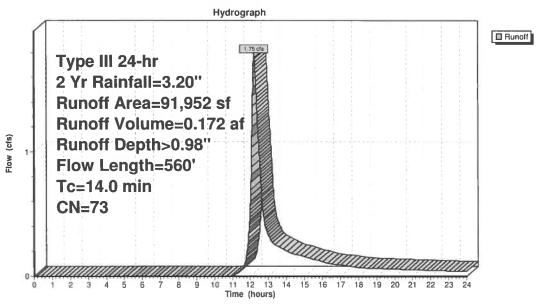
Summary for Subcatchment P3: Post Dev

1.75 cfs @ 12.21 hrs, Volume=

0.172 af, Depth> 0.98"

A	rea (sf)	CN	Description		
	62,580	72	Woods/gra	ss comb., G	Good, HSG C
	29,372	74	>75% Gras	s cover, Go	ood, HSG C
	91,952	73	Weighted A	verage	
	91,952		100.00% P	ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
10.8	50	0.0100	0.08		Sheet Flow, A-B
3.2	510	0.0280	2.69		Grass: Dense n= 0.240 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
14.0	560	Total			

Subcatchment P3: Post Dev



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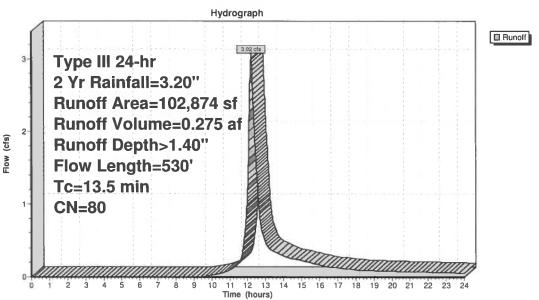
Summary for Subcatchment P4: Post Dev

Runoff = 3.02 cfs @ 12.19 hrs, Volume=

0.275 af, Depth> 1.40"

A	rea (sf)	CN D	escription							
	12.535	98 P	98 Paved parking, HSG C							
	13,138		aved road							
	77,201	74 >	75% Grass	s cover, Go	od, HSG C					
	02.874	80 V	/eighted A	verage						
	77,201			vious Area						
	25,673	2	4.96% lmp	ervious Are	ea					
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
10.8	50	0.0100	0.08		Sheet Flow, A-B					
					Grass: Dense n= 0.240 P2= 3.20"					
1.1	150	0.0200	2.28		Shallow Concentrated Flow, B-C					
					Unpaved Kv= 16.1 fps					
1.0	160	0.0170	2.65		Shallow Concentrated Flow, C-D					
					Paved Kv= 20.3 fps					
0.6	170	0.0100	4.54	3.56						
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'					
					n= 0.013					
13.5	530	Total								

Subcatchment P4: Post Dev



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Summary for Subcatchment P5: Roof

Runoff

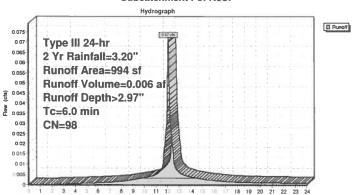
0.07 cfs @ 12.08 hrs, Volume=

0.006 af, Depth> 2.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Yr Rainfall=3.20"

	A	rea (sf)	CN	Description			
		994	98	Roofs, HSC	à A		
		994		100.00% In	npervious A	rea	
(n	Tc nin)	Length (feet)	Slop (ft/fi		Capacity (cfs)	Description	
	6.0					Direct Entry,	

Subcatchment P5: Roof



Summary for Pond 1P: Drain Basin

Inflow Area =

Inflow

2.362 ac, 24.96% Impervious, Inflow Depth > 1.40" for 2 Yr event
3.02 cfs @ 12.19 hrs, Volume= 0.275 af
0.69 cfs @ 12.73 hrs, Volume= 0.215 af, Atten= 77%, Lag= 32.6 min 3.02 cfs @ 12.19 hrs, Volume= 0.69 cfs @ 12.73 hrs, Volume= 0.04 cfs @ 12.73 hrs, Volume= Outflow

0.030 af Discarded = Primary 0.65 cfs @ 12.73 hrs, Volume= 0.185 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 280.73' @ 12.73 hrs Surf.Area= 4,280 sf Storage= 5,028 cf

Plug-Flow detention time= 164.9 min calculated for 0.214 af (78% of inflow) Center-of-Mass det. time= 82.0 min (929.8 - 847.9)

Volume	Invert	Avail.9	Storage	Storage Description				
#1	278.80'	22	2,321 cf	Custom Stage Data	(Irregular) Listed	below (Recalc)	x 1.25	
	_							
Elevation	on Su	ırf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area		
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)		
278.8	30	236	73.0	0	0	236		
279.0	00	950	223.0	111	111	3,769		
280.0	00	2,622	260.0	1,717	1,827	5,212		
281.0	00	3,750	285.0	3,169	4,997	6,330		
281.1	10	5,052	379.0	438	5,435	11,297		
282.0	00	6,503	376.0	5,186	10,621	11,681		
283.0	00	7,994	400.0	7,236	17,857	13,213		
Device	Routing	Inve	ert Outle	et Devices				
#1	Discarded	278.8	0' 0.27	in/hr Exfiltration o	ver Surface area	Conductivity to	Groundwater Elevation = 276.00'	
#2	Primary	278.8	0' 18.0	Round Culvert L	= 25.0' RCP, squ	are edge headwa	all, Ke= 0.500	
	-		Inlet	/ Outlet Invert= 278.	80' / 277.50' S= 0	.0520 '/' Cc= 0.	.900 n= 0.013, Flow Area= 1.77 sf	
#3	Device 2	280.0	0' 6.0"	Vert. Orifice/Grate	C= 0.600			
#4	Device 2	280.9	0' 1.0'	ong Sharp-Crested	Rectangular Weir	2 End Contrac	tion(s) 2.1' Crest Height	
					-			

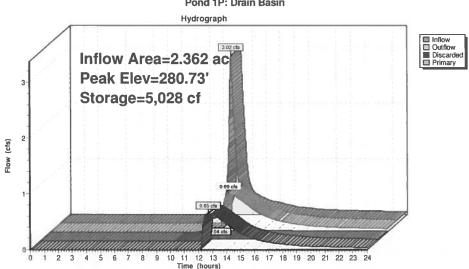
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Discarded OutFlow Max=0.04 cfs @ 12.73 hrs HW=280.73' (Free Discharge) 1=Exfiltration (Controls 0.04 cfs)

Primary OutFlow Max=0.65 cfs @ 12.73 hrs HW=280.73' (Free Discharge) -2=Culvert (Passes 0.65 cfs of 9.24 cfs potential flow)

-3=Orifice/Grate (Orifice Controls 0.65 cfs @ 3.33 fps) 4=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 1P: Drain Basin



Summary for Pond 2P: Roof Runoff

Inflow Area =

Inflow

 0.023 ac,100.00% Impervious, Inflow Depth > 2.97" for 2 Yr event

 0.07 cfs @ 12.08 hrs, Volume=
 0.006 af

 0.05 cfs @ 12.16 hrs, Volume=
 0.006 af, Atten= 28%, Lag=

 0.05 cfs @ 12.16 hrs, Volume=
 0.006 af

 Outflow 0.006 af, Atten= 28%, Lag= 4.5 min Discarded =

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 200.55' @ 12.16 hrs Surf.Area= 50 sf Storage= 11 cf

Plug-Flow detention time= 0.8 min calculated for 0.006 af (100% of inflow) Center-of-Mass det. time= 0.8 min (756.7 - 755.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	200.00	35 cf	5.00'W x 10.00'L x 2.04'H Field A
			102 cf Overall - 15 cf Embedded = 87 cf x 40.0% Voids
#2A	200.50'	15 cf	Cultec C-100HD Inside #1
			Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf
			Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap
			Row Length Adjustment= +0.50' x 1.86 sf x 1 rows
		50 cf	Total Available Storage

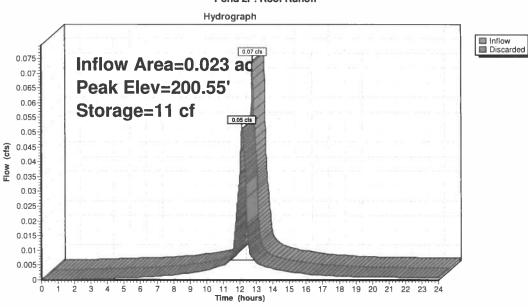
Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	200.00"	27.000 in/hr Exfiltration over Wetted area	Conductivity to Groundwater Elevation = 198.00'

Discarded OutFlow Max=0.05 cfs @ 12.16 hrs HW=200.55' (Free Discharge) 1=Exfiltration (Controls 0.05 cfs)

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Pond 2P: Roof Runoff



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Summary for Link 1L: PreDev

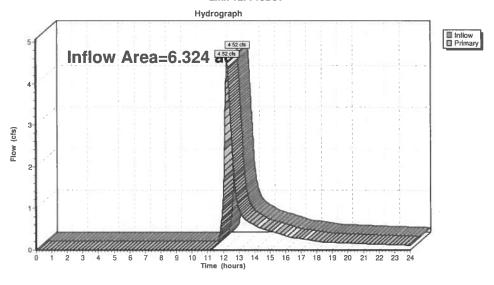
Inflow Area = 6.324 ac, 0.00% Impervious, Inflow Depth > 0.93" for 2 Yr event

Inflow 0.488 af

4.52 cfs @ 12.25 hrs, Volume= 4.52 cfs @ 12.25 hrs, Volume= 0.488 af, Atten= 0%, Lag= 0.0 min Primary

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 1L: PreDev



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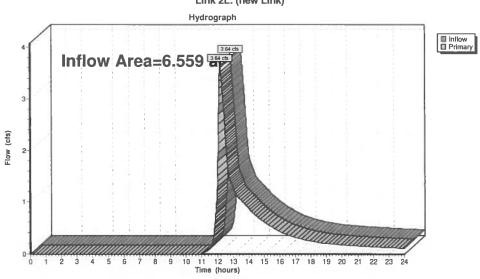
Summary for Link 2L: (new Link)

Inflow Area =

6.559 ac, 8.99% Impervious, Inflow Depth > 0.96" for 2 Yr event 3.64 cfs @ 12.18 hrs, Volume= 0.527 af 3.64 cfs @ 12.18 hrs, Volume= 0.527 af, Atten= 0%, Lag= 0 Inflow Primary 0.527 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 2L: (new Link)



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Summary for Subcatchment E1: PreDev

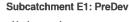
5.94 cfs @ 12.22 hrs, Volume=

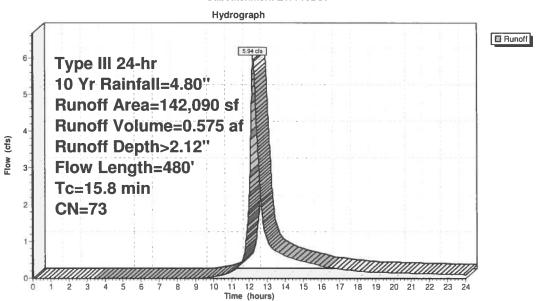
0.575 af, Depth> 2.12"

Runoff by SCS TR-20 method, UH \pm SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Yr Rainfall=4.80"

Ar	ea (sf)	CN	Description		
	5,670	98	Paved park	ing, HSG C	
13	36,420	72	Woods/gras	ss comb., G	ood, HSG C
1-	42.090	73	Weighted A	verage	
13	136.420 96.01% Pervious Area				
	5,670 3.99% Impervious Area			ervious Area	l .
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
13.5	50	0.0160	0.06		Sheet Flow, A-B
0.6	130	0.0500	3.60		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C
1.7	300	0.0200	2.87		Unpaved Kv= 16.1 fps Shallow Concentrated Flow, C-D Paved Kv= 20.3 fps
15.8	480	Total			

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Summary for Subcatchment E2: PreDev

Runoff = 7.78 cfs @ 12.22 hrs, Volume=

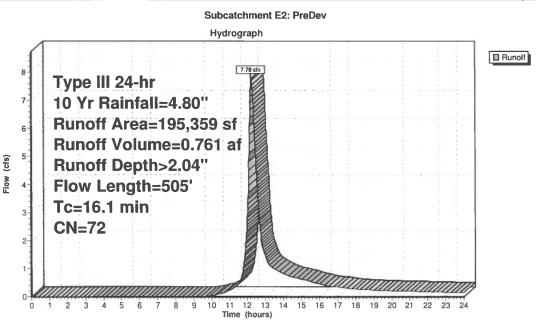
0.761 af, Depth> 2.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24,00 hrs, dt= 0.01 hrs Type III 24-hr 10 Yr Rainfall=4.80"

A	rea (sf)	CN D	escription			
	195,359	72 V	loods/gras	s comb., G	lood, HSG C	
	195,359	1	00.00% Pe	ervious Are	a	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
13.2	50	0.0170	0.06		Sheet Flow, A-B	
2.2	270	0.0160	2.04		Woods: Light underbrush n= 0.400 Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps	P2= 3.20"
0.7	185	0.0800	4.55		Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps	
16.1	505	Total			-	

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Type III 24-hr 10 Yr Rainfall=4.80" Printed 5/6/2020 Page 26



Summary for Subcatchment E3: PreDev

2.97 cfs @ 12.27 hrs, Volume=

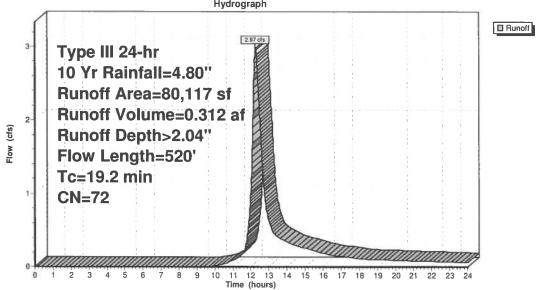
0.312 af, Depth> 2.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Yr Rainfall=4.80"

	Area (sf)	CN D	escription						
	80,117 72 Woods/grass comb., Good, HSG C								
	80,117	1	00.00% P	ervious Are	a				
T (mir	c Length	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
16.	3 50	0.0100	0.05		Sheet Flow, A-B				
2.	9 470	0.0280	2.69		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps				
19.	2 520	Total							

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Subcatchment E3: PreDev

Summary for Subcatchment P1: Post Dev

5.63 cfs @ 12.20 hrs, Volume=

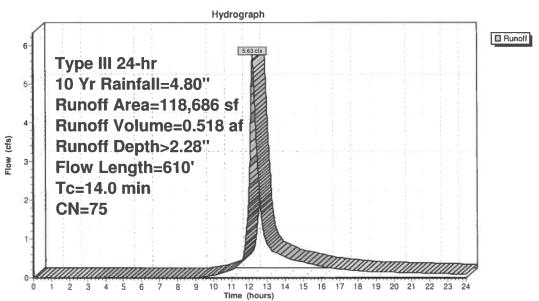
0.518 af, Depth> 2.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Yr Rainfall=4.80"

	Area (sf)	CN	Description		
	0	98			
	8,060	98	Paved park	ing, HSG C	
	51,270	74	>75% Ġras	s cover, Go	od, HSG C
	59,356	72	Woods/gra	ss comb., C	Good, HSG C
	118,686	75	Weighted A	verage	
	110,626			rvious Area	
	8,060		6.79% Impe	ervious Are	
T	c Length	Slope	Velocity	Capacity	Description
(min) (feet)	(ft/ft)	(ft/sec)	(cfs)	
10.	8 50	0.0100	0.08		Sheet Flow, A-B
					Grass: Dense n= 0.240 P2= 3.20"
0.	6 110	0.0400	3.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.	6 450	0.0200	2.87		Shallow Concentrated Flow, C-D
					Paved Kv= 20.3 fps
14.	0 610	Total			

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Subcatchment P1: Post Dev



Summary for Subcatchment P2: Post Dev

Runoff = 4.46 cfs @ 12.15 hrs, Volume=

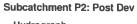
0.369 af, Depth> 2.12"

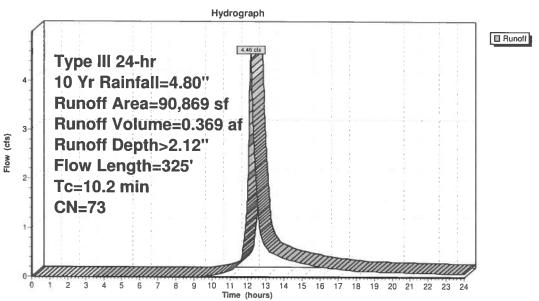
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Yr Rainfall=4.80"

_	Α	rea (sf)	CN	Description					
		43,772		_					
_	43,772 72 Woods/grass comb., G 47,097 74 >75% Grass cover, Go					ood, HSG C			
	90,869 73 90,869			73 Weighted Average 100.00% Pervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
	9.2	50	0.0150	0.09		Sheet Flow, A-B		_	
	1.0	275	0.0800	4.55		Grass: Dense n= 0.240 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps			
	10.2	325	Total				· · · · · · · · · · · · · · · · · · ·	_	

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Type III 24-hr 10 Yr Rainfall=4.80" Printed 5/6/2020 Page 32





Summary for Subcatchment P3: Post Dev

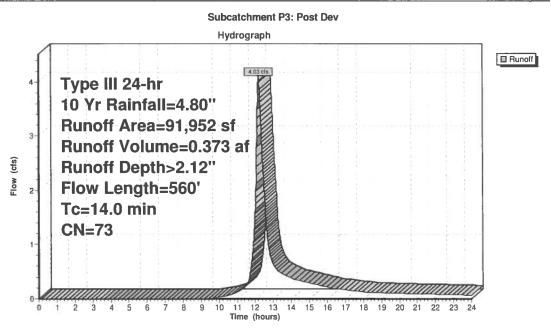
Runoff = 4.03 cfs @ 12.20 hrs, Volume=

0.373 af, Depth> 2.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Yr Rainfall=4.80"

Α	rea (sf)	CN	Description	scription							
	62,580	72	Woods/gra	oods/grass comb., Good, HSG C							
	29,372	74	>75% Gras	s cover, Go	od, HSG C						
91,952 73 Weighted Average											
91,952 100.00% Pervious Area											
Tc	Length	Slope			Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
10.8	50	0.0100	0.08		Sheet Flow, A-B						
					Grass: Dense n= 0.240 P2= 3.20"						
3.2	510	0.0280	2.69		Shallow Concentrated Flow, B-C						
					Unpaved Kv= 16.1 fps						
14.0	560	Total									

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Summary for Subcatchment P4: Post Dev

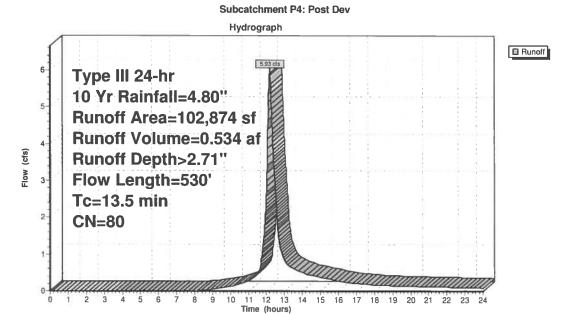
Runoff = 5.93 cfs @ 12.19 hrs, Volume=

0.534 af, Depth> 2.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Yr Rainfall=4.80"

A	rea (sf)	CN D	escription					
	12,535 98 Paved parking, HSG C							
13,138 98 Paved roads HSG C								
	77,201	74 >	od, HSG C					
1	02,874	80 V	Veighted A	verage				
	77,201	7	5.04% Per	vious Area				
	25,673	2	4.96% Imp	pervious Are	ea ea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)				
10.8	50	0.0100	0.08		Sheet Flow, A-B			
					Grass: Dense n= 0.240 P2= 3.20"			
1.1	150	0.0200	2.28		Shallow Concentrated Flow, B-C			
					Unpaved Kv= 16.1 fps			
1.0	160	0.0170	2.65		Shallow Concentrated Flow, C-D			
					Paved Kv= 20.3 fps			
0.6	170	0.0100	4.54	3.56				
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
					n= 0.013			
13.5	530	Total						

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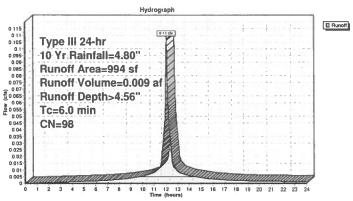
Summary for Subcatchment P5: Roof

Runoff 0.11 cfs @ 12.08 hrs, Volume= 0.009 af, Depth> 4.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Yr Rainfall=4.80"

1	Area (sf)	CN	Description						
	994 98 Roofs, HSG A								
	994		100.00% In	npervious A	rea				
To (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description				
6.0					Direct Entry.				

Subcatchment P5: Roof



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Summary for Pond 1P: Drain Basin

Inflow Area =

Inflow

2.362 ac, 24.96% Impervious, Inflow Depth > 2.71" for 10 Yr event 5.93 cfs @ 12.19 hrs, Volume= 0.534 af 2.25 cfs @ 12.56 hrs, Volume= 0.469 af, Atten= 62%, Lag= 2 0.06 cfs @ 12.56 hrs, Volume= 0.037 af 0.469 af, Atten= 62%, Lag= 22.2 min Outflow

Discarded = Primary 2.20 cfs @ 12.56 hrs, Volume=

Device 2

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 281.43' @ 12.56 hrs Surf.Area= 6,956 sf Storage= 8,992 cf

Plug-Flow detention time= 121.8 min calculated for 0.469 af (88% of inflow) Center-of-Mass det. time= 66.9 min (895.7 - 828.9)

Volume	Invert	Avail.Storage		Storage Description						
#1 278.80' 22,321 cf		Custom Stage Data (Irregular) Listed below (Recalc) x 1.25								
e-,		4.4		4 0	0 0	144 4 4				
Elevatio	n Su	ırf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area				
(feet	t)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)				
278.8	0	236	73.0	0	0	236				
279.0	0	950	223.0	111	111	3,769				
280.0	0	2,622	260.0	1,717	1,827	5,212				
281.0	0	3,750	285.0	3,169	4,997	6,330				
281.1	0	5,052	379.0	438	5,435	11,297				
282.0	0	6,503	376.0	5,186	10,621	11,681				
283.0	0	7,994	400.0	7,236	17,857	13,213				
Device	Routing	Inve	t Outle	et Devices						
#1	Discarded	278.80	0.27	in/hr Exfiltration o	ver Surface area	Conductivity to	Groundwater Elevation = 276.00'			
#2	Primary	278.80)' 18.0'	' Round Culvert L	= 25.0' RCP, squ	are edge headw	all, Ke= 0.500			
							.900 n= 0.013, Flow Area= 1.77 sf			
#3	Device 2	280.00	0' 6.0"	Vert. Orifice/Grate	C = 0.600					

280.90' 1.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s) 2.1' Crest Height

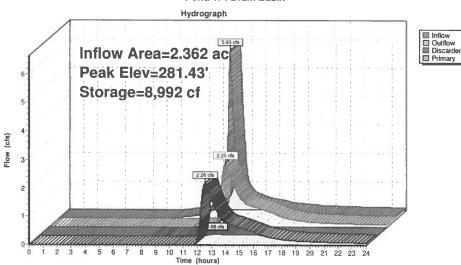
Discarded OutFlow Max=0.06 cfs @ 12.56 hrs HW=281.43' (Free Discharge) 1=Exfiltration (Controls 0.06 cfs)

Primary OutFlow Max=2.19 cfs @ 12.56 hrs HW=281.43' (Free Discharge)

2=Culvert (Passes 2.19 cfs of 11.67 cfs potential flow)
3=Orifice/Grate (Orifice Controls 1.03 cfs @ 5.23 fps)

-4=Sharp-Crested Rectangular Weir (Weir Controls 1.17 cfs @ 2.46 fps)

Pond 1P: Drain Basin



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Summary for Pond 2P: Roof Runoff

Inflow Area = 0.023 ac,100.00% Impervious, Inflow Depth > 4.56" for 10 Yr event

0.11 cfs @ 12.08 hrs, Volume= 0.07 cfs @ 12.17 hrs, Volume= Inflow 0.009 af

Outflow 0.009 af, Atten= 34%, Lag= 5.3 min

Discarded = 0.07 cfs @ 12.17 hrs, Volume= 0.009 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 201.02' @ 12.17 hrs Surf.Area= 50 sf Storage= 27 cf

Plug-Flow detention time= 1.6 min calculated for 0.009 af (100% of inflow)

Center-of-Mass det. time= 1.6 min (749.8 - 748.2)

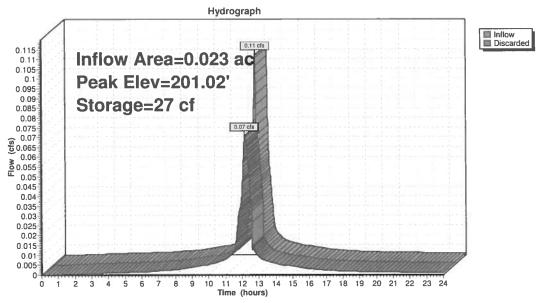
Volume	Invert	Avail.Storage	Storage Description
#1A	200.00'	5.00'W x 10.00'L x 2.04'H Field A	
			102 cf Overall - 15 cf Embedded = 87 cf x 40.0% Voids
#2A	200.50'	15 cf	Cultec C-100HD Inside #1
			Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf
			Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap
			Row Length Adjustment= +0.50' x 1.86 sf x 1 rows
		50 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices				
#1	Discarded	200.00'	27.000 in/hr Exfiltration over Wetted area	Conductivity to Groundwater Elevation = 198.00'			

Discarded OutFlow Max=0.07 cfs @ 12.17 hrs HW=201.02' (Free Discharge) -1=Exfiltration (Controls 0.07 cfs)

Pond 2P: Roof Runoff



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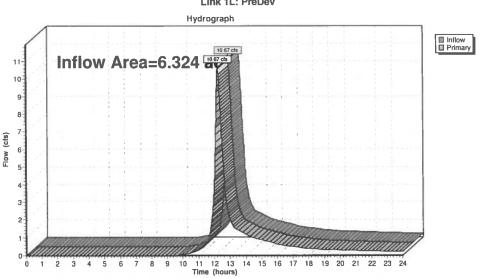
Type III 24-hr 10 Yr Rainfall=4.80" Printed 5/6/2020 Page 42

Summary for Link 1L: PreDev

| Inflow Area = | 6.324 ac, 0.00% Impervious, Inflow Depth > 2.04" | for 10 Yr event | 10.67 cfs @ 12.24 hrs, Volume= 1.073 af | 10.67 cfs @ 12.24 hrs, Volume= 1.073 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 1L: PreDev



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Summary for Link 2L: (new Link)

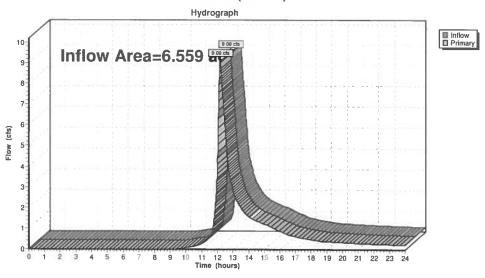
6.559 ac, 8.99% Impervious, Inflow Depth > 2.15" for 10 Yr event 9.09 cfs @ 12.18 hrs, Volume= 1.174 af 9.09 cfs @ 12.18 hrs, Volume= 1.174 af, Atten= 0%, Lag= 0.0 Inflow Area =

Inflow

Primary 1.174 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 2L: (new Link)



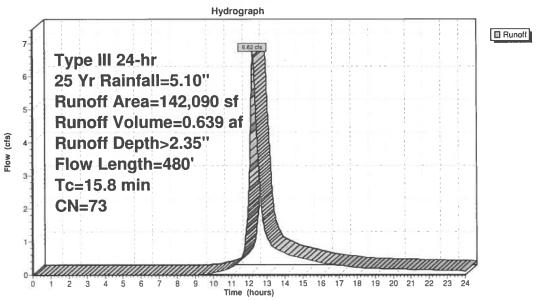
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Summary for Subcatchment E1: PreDev

Runoff 6.62 cfs @ 12.22 hrs, Volume= 0.639 af, Depth> 2.35"

_	A	rea (sf)	CN	Description		
5,670 98 Paved parking, HSG C						
_	1	36,420	Good, HSG C			
	1	42,090	73	Weighted A	verage	
	1	36,420		96.01% Pe	vious Area	
		5,670		3.99% Imp	ervious Area	1
	_					
	Tc	Length	Slope		, ,	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	13.5	50	0.0160	0.06		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	0.6	130	0.0500	3.60		Shallow Concentrated Flow, B-C
						Unpaved Kv= 16.1 fps
	1.7	300	0.0200	2.87		Shallow Concentrated Flow, C-D
_						Paved Kv= 20.3 fps
	15.8	480	Total			

Subcatchment E1: PreDev



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Type III 24-hr 25 Yr Rainfall=5.10" Printed 5/6/2020 Page 46

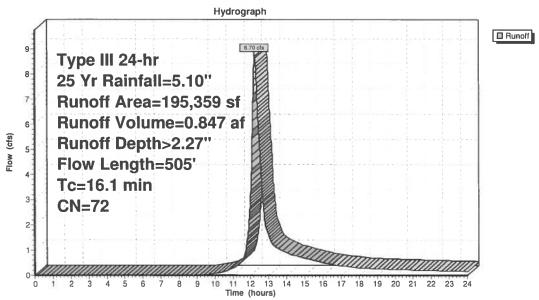
Summary for Subcatchment E2: PreDev

Runoff = 8.70 cfs @ 12.22 hrs, Volume=

0.847 af, Depth> 2.27"

	Α	rea (sf)	CN I	Description		
	1	95,359	72 \	Noods/gras	ss comb., G	ood, HSG C
	1	95,359		a		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	13.2	50	0.0170	0.06		Sheet Flow, A-B
	2.2	270	0.0160	2.04		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	0.7	185	0.0800	4.55		Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps
	16.1	505	Total			

Subcatchment E2: PreDev



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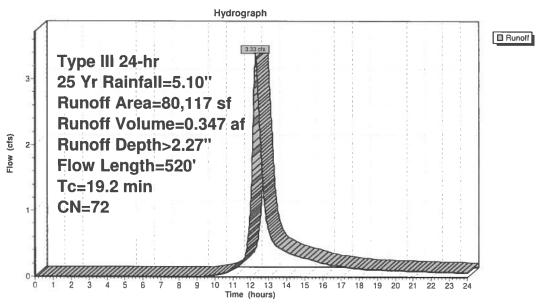
Summary for Subcatchment E3: PreDev

Runoff = 3.33 cfs @ 12.27 hrs, Volume=

0.347 af, Depth> 2.27"

	Α	rea (sf)	CN D	escription			
80,117 72 Woods/grass comb., Good, HSG C							
		80,117	1	00.00% Pe	ervious Are	a	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
•	16.3	50	0.0100	0.05		Sheet Flow, A-B	
	2.9	470	0.0280	2.69		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps	
	10.2	520	Total				

Subcatchment E3: PreDev



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Type III 24-hr 25 Yr Rainfall=5.10" Printed 5/6/2020 Page 50

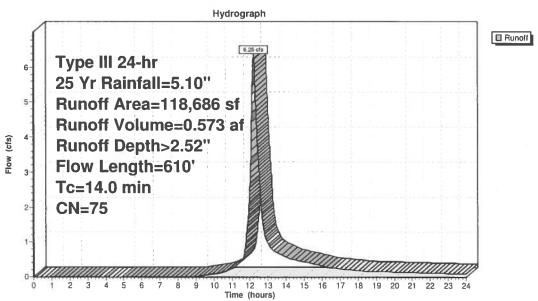
Summary for Subcatchment P1: Post Dev

Runoff = 6.25 cfs @ 12.20 hrs, Volume=

0.573 af, Depth> 2.52"

	A	rea (sf)	CN I	Description									
*		0	98										
		8,060	98	aved park	ved parking, HSG C								
		51,270		>75% Gras									
_		59,356	72	Noods/gra	ss comb., C	lood, HSG C							
		18,686		Neighted A									
	1	10,626			rvious Area								
		8,060	-	5.79% Impe	ervious Are	a							
	Тс	Length	Slope		Capacity	Description							
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			_					
	10.8	50	0.0100	0.08		Sheet Flow, A-B							
	0.6	110	0.0400	3.22		Grass: Dense n= 0.240 P2= 3.20" Shallow Concentrated Flow, B-C							
	2.6	450	0.0200	2.87		Unpaved Kv= 16.1 fps Shallow Concentrated Flow, C-D Paved Kv= 20.3 fps							
	14.0	610	Total					_					

Subcatchment P1: Post Dev



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Type III 24-hr 25 Yr Rainfall=5.10" Printed 5/6/2020 Page 52

Summary for Subcatchment P2: Post Dev

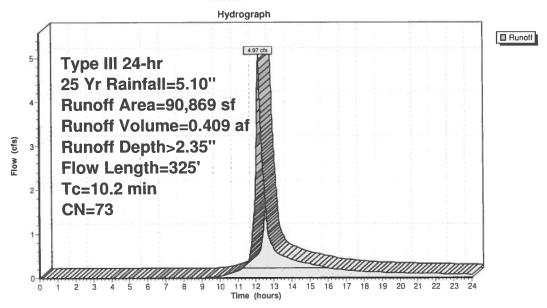
Runoff = 4.97 cfs @ 12.14 hrs, Volume=

0.409 af, Depth> 2.35"

	Α	rea (sf)	CN D	Description						
	43,772 72 Woods/grass comb., Good, HSG C									
47,097 74 >75% Grass cover, Good, HSG C										
90,869 73 Weighted Average										
		90,869	1	00.00% P	ervious Are	a				
		Length	Slope	Velocity	Capacity	Description				
(п	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	9.2	50	0.0150	0.09		Sheet Flow, A-B				
						Grass: Dense n= 0.240 P2= 3.20"				
	1.0	275	0.0800	4.55		Shallow Concentrated Flow, B-C				
						Unpaved Kv= 16.1 fps				
1	0.2	325	Total							

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Subcatchment P2: Post Dev



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Type III 24-hr 25 Yr Rainfall=5.10" Printed 5/6/2020 Page 54

Summary for Subcatchment P3: Post Dev

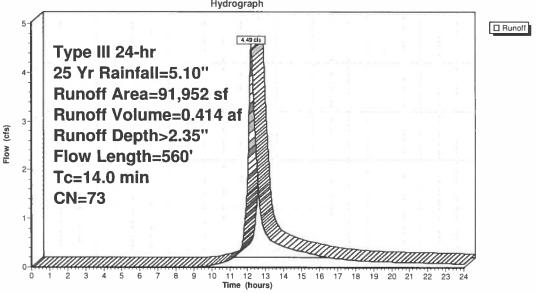
4.49 cfs @ 12.20 hrs, Volume= Runoff

0.414 af, Depth> 2.35"

	A	rea (sf)	CN E	Description							
		52,580 72 Woods/grass comb., Good, HSG C									
		29,372	74 >	75% Gras	s cover, Go	od, HSG C					
		91,952	73 V	Veighted A	verage						
		91,952	1	00.00% Pe	ervious Are	a					
		Length	Slope	Velocity	Capacity	Description					
(ı	min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	10.8	50	0.0100	0.08		Sheet Flow, A-B					
	3.2	510	0.0280	2.69		Grass: Dense n= 0.240 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps					
	14.0	560	Total								

Subcatchment P3: Post Dev





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Type III 24-hr 25 Yr Rainfall≃5.10" Printed 5/6/2020 Page 56

Summary for Subcatchment P4: Post Dev

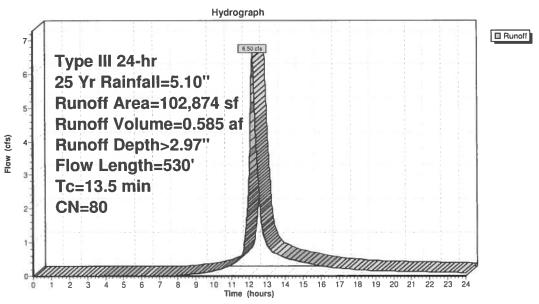
6.50 cfs @ 12.19 hrs, Volume=

0.585 af, Depth> 2.97"

A	rea (sf)	CN D	CN Description									
	12,535	98 P	aved park	ing, HSG C								
	13,138	98 P	aved road	s HSG C								
	77,201	74 >	75% Gras	s cover, Go	od, HSG C							
1	02,874	80 V	Veighted A	verage								
	77,201			vious Area								
	25.673			ervious Are								
	,											
Tc	Length	Slope	Velocity	Capacity	Description							
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	occupación de la company de la							
10.8	50	0.0100	0.08	11	Sheet Flow, A-B							
					Grass: Dense n= 0.240 P2= 3,20"							
1.1	150	0.0200	2.28		Shallow Concentrated Flow, B-C							
					Unpaved Kv= 16.1 fps							
1.0	160	0.0170	2.65		Shallow Concentrated Flow, C-D							
					Paved Kv= 20.3 fps							
0.6	170	0.0100	4.54	3.56	Pipe Channel, D-E							
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'							
					n= 0.013							
13.5	530	Total										

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Subcatchment P4: Post Dev



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Type III 24-hr 25 Yr Rainfall=5.10" Printed 5/6/2020 Page 58

Summary for Subcatchment P5: Roof

Runoff

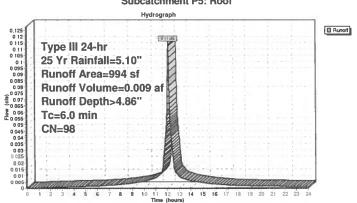
0.11 cfs @ 12.08 hrs, Volume=

0.009 af, Depth> 4.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 25 Yr Rainfall=5.10"

Α	rea (sf)	CN	Description							
	994 98 Roofs, HSG A									
	994 100.00% Impervious Area									
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description					
6.0					Direct Entry					

Subcatchment P5: Roof



Summary for Pond 1P: Drain Basin

Inflow Area =

Inflow

Outflow 0.520 af, Atten= 60%, Lag= 21.2 min

0.06 cfs @ 12.54 hrs, Volume= Discarded = 0.038 af Primary 2.54 cfs @ 12.54 hrs, Volume= 0.482 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 281.53' @ 12.54 hrs Surf.Area= 7,147 sf Storage= 9,665 cf

Plug-Flow detention time= 116.8 min calculated for 0.520 af (89% of inflow) Center-of-Mass det. time= 65.0 min (891.3 - 826.3)

Volume	/olume Invert Avail.Storage		Storage Description	1				
#1	278.80	22	2,321 cf	Custom Stage Data	a (Irregular) Listed	below (Recalc)	x 1.25	_
Elevation	on Si	urf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area		
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)		
278.8	30	236	73.0	0	0	236		
279.0	00	950	223.0	111	111	3,769		
280.0	00	2,622	260.0	1,717	1,827	5,212		
281.0	00	3,750	285.0	3,169	4,997	6,330		
281.1	10	5,052	379.0	438	5,435	11,297		
282.0	00	6,503	376.0	5,186	10,621	11,681		
283.0	00	7,994	400.0	7,236	17,857	13,213		
Device	Routing	Inve	ert Outle	et Devices				
#1	Discarded	278.8	0.27	0 in/hr Exfiltration of	ver Surface area	Conductivity to	Groundwater Elevation = 276.00'	_
#2	Primary	278.8	0' 18.0 '	" Round Culvert L	= 25.0' RCP, squ	are edge headwa	all, Ke= 0.500	
	•		Inlet	/ Outlet Invert= 278.	.80' / 277.50' S= 0	0.0520 T Cc= 0.	.900 n= 0.013, Flow Area= 1.77 sf	
#3	Device 2	280.0	10' 6.0 "	Vert. Orifice/Grate	C= 0.600		,	
#4	Device 2	280.9	0' 1.0'1	ong Sharp-Crested	Rectangular Weir	2 End Contrac	tion(s) 2.1' Crest Height	
					_			

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Discarded OutFlow Max=0.06 cfs @ 12.54 hrs HW=281.53' (Free Discharge) 1=Exfiltration (Controls 0.06 cfs)

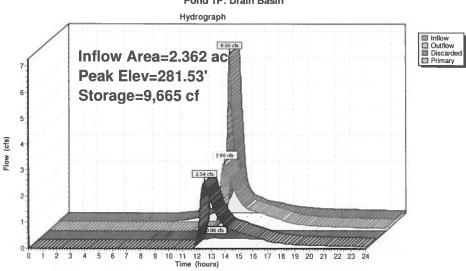
Primary OutFlow Max=2.54 cfs @ 12.54 hrs HW=281.53' (Free Discharge)

2=Culvert (Passes 2.54 cfs of 11.96 cfs potential flow)

-3=Orifice/Grate (Orifice Controls 1.07 cfs @ 5.44 fps)

-4=Sharp-Crested Rectangular Weir (Weir Controls 1.47 cfs @ 2.68 fps)

Pond 1P: Drain Basin



Summary for Pond 2P: Roof Runoff

Inflow Area =

0.023 ac,100.00% Impervious, Inflow Depth > 4.86" for 25 Yr event 0.11 cfs @ 12.08 hrs, Volume= 0.009 af

Inflow Outflow 0.11 cfs @ 12.08 hrs, Volume= 0.07 cfs @ 12.17 hrs, Volume=

0.009 af, Atten= 34%, Lag= 5.3 min

Discarded =

0.07 cfs @ 12.17 hrs, Volume=

0.009 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 201.12' @ 12.17 hrs Surf.Area= 50 sf Storage= 29 cf

Plug-Flow detention time= 1.8 min calculated for 0.009 af (100% of inflow) Center-of-Mass det. time= 1.7 min (748.9 - 747.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	200.00'	35 cf	5.00'W x 10.00'L x 2.04'H Field A
			102 cf Overall - 15 cf Embedded = 87 cf x 40.0% Voids
#2A	200.50'	15 cf	Cultec C-100HD Inside #1
			Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50'L = 14.0 cf
			Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap
			Row Length Adjustment= +0.50' x 1.86 sf x 1 rows
		50 cf	Total Available Storage

Storage Group A created with Chamber Wizard

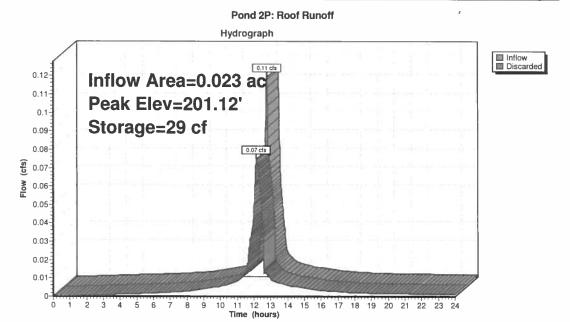
Device Routing Invert Outlet Devices

#1 Discarded

200.00' 27.000 in/hr Exfiltration over Wetted area Conductivity to Groundwater Elevation = 198.00'

Discarded OutFlow Max=0.07 cfs @ 12.17 hrs HW=201.12' (Free Discharge) 1-1=Exfiltration (Controls 0.07 cfs)

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Summary for Link 1L: PreDev

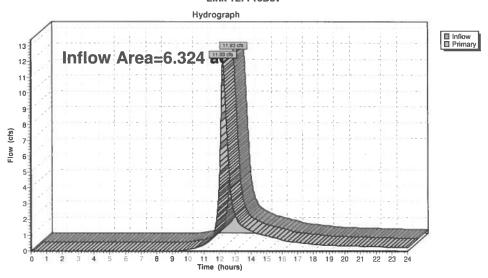
6.324 ac, 0.00% Impervious, Inflow Depth > 2.27" for 25 Yr event 11.93 cfs @ 12.24 hrs, Volume= 1.194 af Inflow Area =

Inflow

Primary 11.93 cfs @ 12.24 hrs, Volume= 1.194 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 1L: PreDev



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Summary for Link 2L: (new Link)

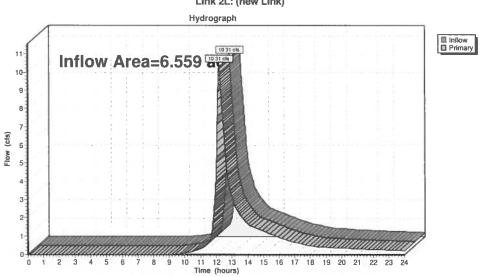
6.559 ac, 8.99% Impervious, Inflow Depth > 2.39" for 25 Yr event 0.31 cfs @ 12.18 hrs, Volume= 1.305 af Inflow Area =

10.31 cfs @ 12.18 hrs, Volume= 10.31 cfs @ 12.18 hrs, Volume=

Inflow Primary 1.305 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 2L: (new Link)



Summary for Subcatchment E1: PreDev

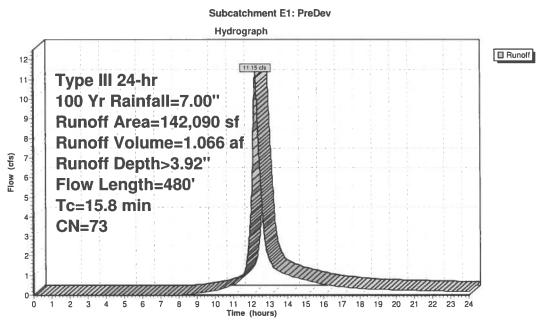
Runoff = 11.15 cfs @ 12.22 hrs, Volume=

1.066 af, Depth> 3.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Yr Rainfall=7.00"

	A	rea (sf)	CN	Description		
		5,670	98	Paved park	ing, HSG C	
	1	36,420	72	Woods/gra	ss comb., G	ood, HSG C
		42,090 36,420 5,670			verage vious Area ervious Area	1
	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
_	13.5	50	0.0160	0.06		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	0.6	130	0.0500	3.60		Shallow Concentrated Flow, B-C
	1.7	300	0.0200	2.87		Unpaved Kv= 16.1 fps Shallow Concentrated Flow, C-D Paved Kv= 20.3 fps
-	15.8	480	Total			

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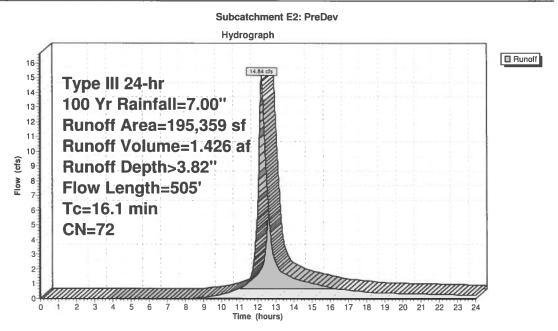
Summary for Subcatchment E2: PreDev

Runoff = 14.84 cfs @ 12.22 hrs, Volume= 1.426 af, Depth> 3.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Yr Rainfall=7.00"

	Area (sf)	CN D	escription								
	195,359	72 V	72 Woods/grass comb., Good, HSG C								
	195,359	1	00.00% Pe	ervious Are	a						
To (min)		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description						
13.2	50	0.0170	0.06		Sheet Flow, A-B						
2.2	270	0.0160	2.04		Woods: Light underbrush n= 0.400 Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps	P2= 3.20"					
0.7	185	0.0800	4.55		Shallow Concentrated Flow, C-D Unpaved Kv= 16.1 fps						
16.1	505	Total									

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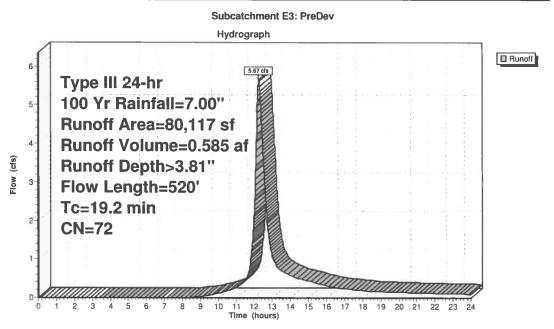
Summary for Subcatchment E3: PreDev

Runoff = 5.67 cfs @ 12.27 hrs, Volume≈ 0.585 af, Depth> 3.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Yr Rainfall=7.00"

_	Α	rea (sf)	CN [Description		
		80,117	72 V	Voods/gras	ss comb., G	Good, HSG C
		80,117	1	00.00% Pe	ervious Area	a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	16.3	50	0.0100	0.05		Sheet Flow, A-B
	2.9	470	0.0280	2.69		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	19.2	520	Total			

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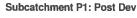
Summary for Subcatchment P1: Post Dev

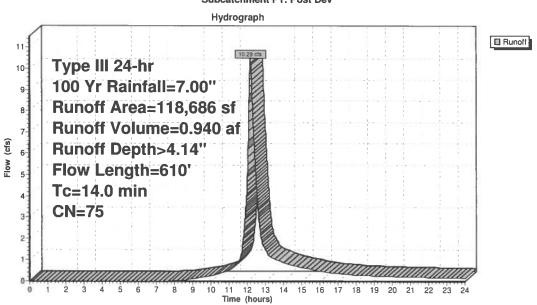
Runoff 10.29 cfs @ 12.19 hrs, Volume= 0.940 af, Depth> 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Yr Rainfall=7.00"

	Aro	a (sf)	CN I	Description										
	AIG	0	98	Jescription		''								
		_												
		3,060												
		1,270												
		9,356				lood, HSG C								
	118	8,686	,686 75 Weighted Average											
	110	0,626	!	93.21% Pervious Area										
	8	8,060	1	6.79% Impervious Area										
	Tc L	ength	Slope	Velocity	Capacity	Description								
(mi	in)	(feet)	(ft/ft)	(ft/sec)	(cfs)									
10	3.8	50	0.0100	0.08		Sheet Flow, A-B								
						Grass: Dense n= 0.240 P2= 3.20"								
	0.6	110	0.0400	3.22		Shallow Concentrated Flow, B-C								
						Unpaved Kv= 16.1 fps								
2	2.6	450	0.0200	2.87		Shallow Concentrated Flow, C-D								
_		.00		2.07		Paved Kv= 20.3 fps								
1/	4.0	610	Total											
		010												

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Summary for Subcatchment P2: Post Dev

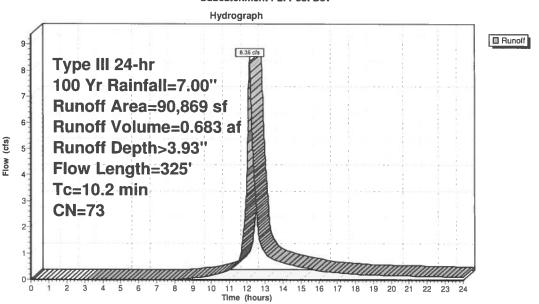
Runoff 8.36 cfs @ 12.14 hrs, Volume= 0.683 af, Depth> 3.93"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Yr Rainfall=7.00"

Α	rea (sf)	CN	Description										
	43,772	72	Woods/gra	ss comb., G	Good, HSG C								
	47,097	74	>75% Gras	5% Grass cover, Good, HSG C									
90,869 73 Weighted Average 90,869 100.00% Pervious Area													
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description								
9.2	50	0.0150	0.09		Sheet Flow, A-B								
1.0	1.0 275 0.0800 4.55				Grass: Dense n= 0.240 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps								
10.2	325	Total											

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Summary for Subcatchment P3: Post Dev

Runoff = 7.56 cfs @ 12.19 hrs, Volume=

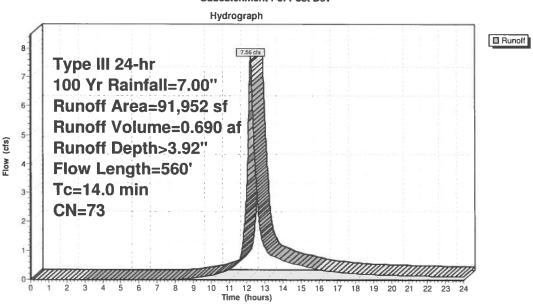
0.690 af, Depth> 3.92"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Yr Rainfall=7.00"

Α	rea (sf)	CN	Description												
	62,580	72	Woods/gra	ods/grass comb., Good, HSG C											
	29.372			5% Grass cover, Good, HSG C											
91,952 73 Weighted Average															
91,952 100.00% Pervious Area															
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description										
10.8		0.0100		(0.0)	Sheet Flow, A-B										
3.2	510	0.0280	2.69		Grass: Dense n= 0.240 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps										
14.0	560	Total													

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Summary for Subcatchment P4: Post Dev

10.16 cfs @ 12.18 hrs, Volume= Runoff

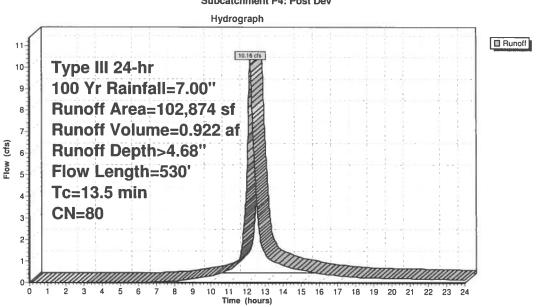
0.922 af, Depth> 4.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Yr Rainfall=7.00"

A	rea (sf)	CN D	escription									
	12,535	98 P	aved park	ng, HSG C								
	13,138	138 98 Paved roads HSG C										
	77,201	74 >	ood, HSG C									
1	02.874	80 V	eighted A	verage								
	77,201			vious Area								
	25,673	2	4.96% Imp	ervious Are	эа							
Tc	Length	Slope	Velocity	Capacity	Description							
(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)								
10.8	50	0.0100	0.08		Sheet Flow, A-B							
					Grass: Dense n= 0.240 P2= 3.20"							
1.1	150	0.0200	2.28		Shallow Concentrated Flow, B-C							
					Unpaved Kv= 16.1 fps							
1.0	160	0.0170	2.65		Shallow Concentrated Flow, C-D							
					Paved Kv= 20.3 fps							
0.6	170	0.0100	4.54	3.56	Pipe Channel, D-E							
12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'												
					n= 0.013							
13.5	530	Total										

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Subcatchment P4: Post Dev



Summary for Subcatchment P5: Roof

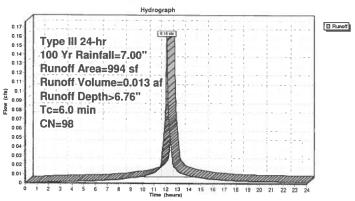
Runoff 0.16 cfs @ 12.08 hrs, Volume=

0.013 af, Depth> 6.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Yr Rainfall=7.00"

Area (st) CN	Description							
99	4 98	Roofs, HS0	àΑ						
99	4	100.00% In	npervious A	rea					
Tc Leng (min) (fee		oe Velocity ft) (ft/sec)	Capacity (cfs)	Description					
6.0				Direct Entry,					





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Type III 24-hr 100 Yr Rainfall=7.00" Printed 5/6/2020 Page 80

Summary for Pond 1P: Drain Basin

Inflow Area = 2.362 ac, 24.96% Impervious, Inflow Depth > 4.68" for 100 Yr event 10.16 cfs @ 12.18 hrs, Volume= 0.922 af 4.69 cfs @ 12.48 hrs, Volume= 0.853 af, Atten= 54%, Lag= 17

Inflow Outflow

0.853 af, Atten= 54%, Lag= 17.9 min 0.044 af

Discarded = 0.07 cfs @ 12.48 hrs, Volume=

Primary 4.61 cfs @ 12.48 hrs, Volume=

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 282.06' @ 12.48 hrs Surf.Area= 8,232 sf Storage= 13,754 cf

Plug-Flow detention time= 95.9 min calculated for 0.852 af (92% of inflow) Center-of-Mass det. time= 57.9 min (871.3 - 813.4)

Volume	Invert	Avail.S	Storage	Storage Description				
#1 278.80' 22,321 cf		,321 cf	Custom Stage Data (Irregular) Listed below (Recalc) x 1.25					
	_							
Elevation		urf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area		
(fee	t)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)		
278.8	-	236	73.0	0	0	236		
279.0		950	223.0	111	111	3,769		
280.0	Ю	2,622	260.0	1,717	1,827	5,212		
281.0	0	3,750	285.0	3,169	4,997	6,330		
281.1	0	5,052	379.0	438	5,435	11,297		
282.0		6,503	376.0	5,186	10,621	11,681		
283.0	Ю	7,994	400.0	7,236	17,857	13,213		
Davida	Davidson	1						
Device	Routing	lnve		et Devices				
#1	Discarded	278.8	0' 0.27	0 in/hr Exfiltration o	ver Surface area	Conductivity to (Groundwater Elevation = 276.00'	
#2	Primary	278.8	0' 18.0 '	" Round Culvert L:	= 25.0' RCP, squa	are edge headwa	all, Ke= 0.500	
			Inlet	/ Outlet Invert= 278.8	80' / 277.50' S= 0	.0520 ¹ /' Cc= 0.	900 n= 0.013, Flow Area= 1.77 sf	
#3	Device 2	280.0	0' 6.0"	Vert. Orifice/Grate	C= 0.600			
#4	Device 2	280.9	0' 1.0' I	long Sharp-Crested	Rectangular Weir	2 End Contract	tion(s) 2.1' Crest Height	
				-			······································	

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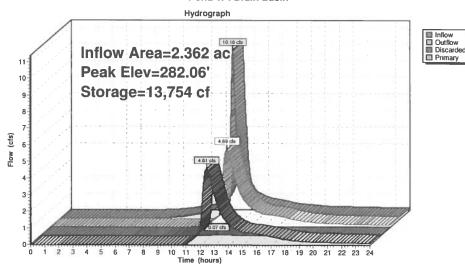
Discarded OutFlow Max=0.07 cfs @ 12.48 hrs HW=282.06' (Free Discharge) 1=Exfiltration (Controls 0.07 cfs)

Primary OutFlow Max=4.61 cfs @ 12.48 hrs HW=282.06' (Free Discharge) 2=Culvert (Passes 4.61 cfs of 13.48 cfs potential flow)

3=Orifice/Grate (Orifice Controls 1.27 cfs @ 6.47 fps)

4=Sharp-Crested Rectangular Weir (Weir Controls 3.34 cfs @ 3.76 fps)

Pond 1P: Drain Basin



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Type III 24-hr 100 Yr Rainfall=7.00" Printed 5/6/2020 Page 82

Summary for Pond 2P: Roof Runoff

Inflow Area = 0.023 ac,100.00% Impervious, Inflow Depth > 6.76" for 100 Yr event 0.013 af 0.013 af, Atten= 31%, Lag= 4.8 min 0.16 cfs @ 12.08 hrs, Volume= 0.11 cfs @ 12.16 hrs, Volume= Inflow Outflow Discarded = 0.11 cfs @ 12.16 hrs, Volume= 0.013 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 201.88' @ 12.16 hrs Surf.Area= 50 sf Storage= 47 cf

Plug-Flow detention time= 2.3 min calculated for 0.013 af (100% of inflow) Center-of-Mass det. time= 2.3 min (744.7 - 742.4)

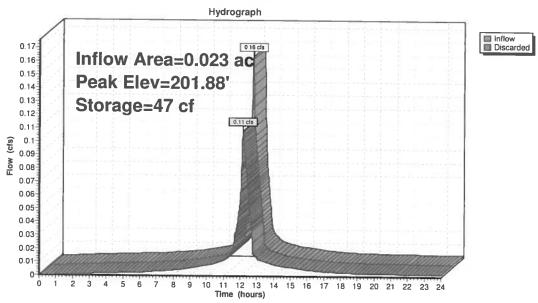
Volume	Invert	Avail.Storage	Storage Description
#1A	200.00'	35 cf	5.00'W x 10.00'L x 2.04'H Field A
			102 cf Overall - 15 cf Embedded = 87 cf x 40.0% Voids
#2A	200.50'	15 cf	Cultec C-100HD Inside #1
			Effective Size= 32.1"W x 12.0"H => 1.86 sf x 7.50"L = 14.0 cf
			Overall Size= 36.0"W x 12.5"H x 8.00'L with 0.50' Overlap
			Row Length Adjustment⇒ +0.50' x 1.86 sf x 1 rows
		50 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	200.00'	27.000 in/hr Exfiltration over Wetted area	Conductivity to Groundwater Elevation = 198.00'

Discarded OutFlow Max=0.11 cfs @ 12.16 hrs HW=201.88' (Free Discharge) -1=Exfiltration (Controls 0.11 cfs)

Pond 2P: Roof Runoff



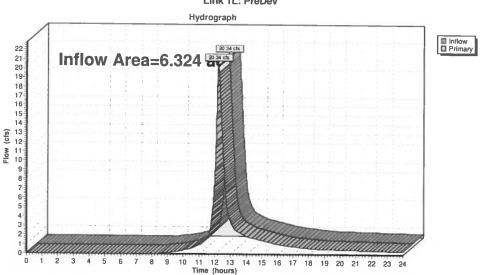
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Type III 24-hr 100 Yr Rainfall=7.00" Printed 5/6/2020 Page 84

Summary for Link 1L: PreDev

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 1L: PreDev



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Summary for Link 2L: (new Link)

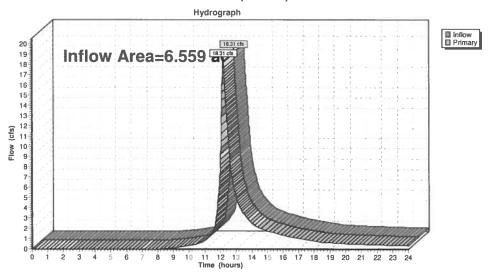
Inflow Area = Inflow = 6.559 ac, 8.99% Impervious, Inflow Depth > 3.99" for 100 Yr event 18.31 cfs @ 12.18 hrs, Volume= 2.182 af 18.31 cfs @ 12.18 hrs, Volume= 2.182 af, Atten= 0%, Lag= 0.0

Primary

2.182 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs

Link 2L: (new Link)



APPENDIX - B

Hydraulic Design (Manning's Equation) Time of Flow, Average CN values Groundwater Mounding Calculations

Standard 2

STORM DRAINAGE CALCULATIONS
Pipe Flow Calculations - Manning's Equation

Project: Town:

Triangle Farm

i = Rainfall Intensity at 25 Year Storm

5/7/20

Date:

7,701 rst

Revised: Job No: Calc. by:

.p.s.)	(f.p.s.) Upper 4.10 284.50 5.60 284.50 3.10 284.20 6.50 283.50 8.60 283.50 8.60 283.50 3.60 282.80
0.020 2.50 4.10 0.040 2.40 5.60	2.50 2.40 5.40 2.20 2.00 8.20 3.40
12 0.00	12 12 12 12 12 12 12
0.49	0.49 0.63 0.66 0.72 1.95
16.12 4.33 23.30 3.67	
0.04	0.04 0.01 1.40 0.03 0.01 0.51
0.41 23.29	0.41 0.44 0.48 0.45 0.46
5 0.42	
DMH 3 5	W 4 4 4 1 1 1
	0.29 0.46 0.46 13.19 0.03 13.22 4.69 0.66 1.05 12 0.005 0.33 0.45 12.34 0.01 12.34 4.81 0.72 12 0.060 0.33 1.26 0.46 24.70 0.51 25.21 3.57 2.05 12 0.005 0.773 0.77 0.56 12.34 0.00 12.34 4.81 1.95 12 0.005

OVERLAND FLOW TRAVEL TIME

STORM RUNOFF DATA

Date: 5/7/20

Revised:

Project: Town: Triangle Farm Holliston, MA

Job No. 7,701

Calc by rst

Structure		Impervious			Lawn			Wooded		Total
	Length (ft)	Slope ('/')	Time (min.)	Length (ft)	Slope ('/')	Time (min.)	Length (ft)	Slope ('/')	Time (min.)	Travel Time (min.)
1	90	0.008	1.60	80	0.020	14.48				16.08
2	90	0.008	1.60	190	0.020	21.69				23.29
5	140	0.017	1.68	60	0.030	11.51				13.19
6	140	0.015	1.77	50	0.030	10.57				12.34
8	140	0.015	1.77	50.00	0.030	10.57				12.34

AVERAGE 'c' VALUE FOR STRUCTURES

STORM RUNOFF DATA Date: 5/7/20 Revised:							
Project: Town:	Triangle Farm Holliston, MA					Job No: Calc. by:	7,701 RST
Structure	Total Area	Ground Cover	Area	С	Σ(Area*c)	Average c	Total Area
	(SF)		(SF)			_	(Ac)
CB#1	9,766	imp	3,058	0.95	2,905.10	0.50	0.224
		lawn	6,708	0.30	2,012.40		
		wooded	0	0.20	0.00		
CB#2	18,259	imp	3,111	0.95	2,955.45	0.41	0.419
		lawn	15,148	0.30	4,544.40		
		wooded	0	0.20	0.00		
CB#5	12,630	imp	3,549	0.95	3,371.55	0.48	0.290
		lawn	9.081	0.30	2,724.30		
		wooded	0	0.20	0.00		
CB#6	14,304	imp	3,399	0.95	3,229.05	0.45	0.328
		lawn	10,905	0.30	3,271.50		
		wooded	0	0.20	0.00		
CB#8	31,753	imp	12,554	0.95	11,926.30	0.56	0.729
		lawn	19,199	0.30	5,759.70		
		wooded	0	0.20	0.00		

APPENDIX - C

Stormwater Recharge Calculations, Water Quality Volumes, TSS Removal & Infiltration BMP Drain Time Groundwater Mounding Calculations

Standards 3 & 4:

APPENDIX – B Stormwater Recharge, Water Quality & Forebay Calculations Standard 3 & 4:

Project:

Triangle Farm Holliston, Massachusetts

Date: May 8, 2020

Water Quality Volume (WQV): Based on 1.0 inch rainfall Recharge Volume(Rv): Based on Soil Classification

Rv = F * Impervious Area

Rv = Required Recharge Volume

F = Depth Factor

Soil Type A – 0.60 inch

Soil Type B - 0.35 inch

Soil Type C - 0.25 inch

Soil Type D - 0.00 inch

Total Impervious Area:

Roadway/Drives:

25,673 s.f. (To drainage basin)

Roadway(bypass basin) 2,390 s.f.

Roof: (to basins)

13,184 s.f.

Total Imp. Area:

41,247 s.f.

Total Impervious to Recharge Basins: 38,857 s.f.

Total Impervious Area Uncaptured:

2,390 s.f.

Capture Adjustment:

38,857 s.f. / 41,247 s.f. = 94.2% > 65%

41,247 s.f. / 38,857 s.f. = 1.06 capture adjustment

Recharge Volume required Roof Area:

Each system captures 50% of the roof area.

Roof Area: (Largest house) 1,988 s.f

Rv = (0.25 inch * 994 s.f.) / 12 = 21 c.f.

Recharge Volume Provided:

Cultec Unit C-100HD w/stone:

Tot. Volume: 50 c.f.

Time to drain:

Drawdown time = Volume/(K*Bottom Area)

Volume = 21 cf

K=0.27 in/hr = 0.023 ft/hr

Bottom Area = 50 sf

Drawdown time = $21/(0.023 \text{ ft/hr } \times 50 \text{ sf})$

Drawdown time = 18 hr < 72 hr ok

Drainage Basin #1:

Imp. Area Pavement: 25,673 s.f.

WQV = (25,673 sf * 1.0 in)/12 = 2139 c.f.

Recharge Volume Required: (Soil Type C – 0.25 inch)

Tot. Imp Area: 25,673 s.f.

 $Rv = (25,673 \text{ sf} * 0.25 \text{ in})/12 = \frac{534 \text{ c.f.}}{2500 \text{ c.f.}} \times Capture Adjustment (1.06) = \frac{567 \text{ c.f.}}{2500 \text{ c.f.}}$

Storage Volume below outlet

"Static" Storage Volume Provided:

Volume (Outlet 280.0) provided = 2,284 c.f.

2,284 > 2,139 c.f. **OK**

Forebay Sizing:

Forebay Volume Required: (Paved Area) x 0.10 inch of runoff

 $(25,673 \text{ s.f. } \times 0.10 \text{ in})/12 = 214 \text{ cu.ft.}$

Forebay Volume Provided:

Elev.	Area	Inc.Store	Cum.Store		
<u>(ft.)</u>	(s.f.)	(cu.ft.)	(cu.ft.)		
280.0	702	0	0		
281.0	1195	950	950		

Total Storage Povided: 950 c.f.

950 cf > 214 cf ok

Time to drain:

Drawdown time = Volume/(K*Bottom Area)

Volume = 2139 cf

K=0.27 in/hr = 0.023 ft/hr

Bottom Area = 2622 sf

Drawdown time = $2139/(0.023 \text{ ft/hr } \times 2622 \text{ sf})$

Drawdown time = 35 hr < 72 hr ok

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

Select BMP from Drop Down MenuAfter BMP is selected, TSS Removal and other Columns are automatically completed.

Separate Form Needs to be Completed for Each Remaining **Outlet or BMP Train** Load (D-E *Equals remaining load from previous BMP (E) 0.75 0.56 0.11 0.11 0.11 Removed (C*D) which enters the BMP Amount 0.25 0.19 0.45 0.00 0.00 %68 Total TSS Removal = Starting TSS Load* 1.00 0.75 0.56 0.11 0.11 TSS Removal Location: Drainage Outlet #9 Rate 0.25 0.25 0.80 0.00 0.00 Project: Triangle Farm Date: 5/8/2020 Prepared By: GLM Deep Sump and Hooded Sediment Forebay Infiltration Basin Catch Basin BMP¹ \mathbf{m} Calculation Worksheet IsvomeA 22T

must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1 Non-automated TSS Calculation Sheet

Mass. Dept. of Environmental Protection

Mound Calculation Basin Triangle Farm, Holliston, MA Date: 05/8/2020

This spreadsheet will calculate the height of a groundwater mound beneath a stormwater infiltration basin. More information can be found in the U.S. Geological Survey Scientific Investigations Report 2010-5102 "Simulation of groundwater mounding beneath hypothetical stormwater infiltration basins"

The user must specify infiltration rate (R), specific yield (Sy), horizontal hydraulic conductivity (Kh), basin dimensions (x, y), duration of infiltration period (t), and the initial thickness of the saturated zone (hi(0), height of the water table if the bottom of the aquifer is the datum). For a square basin the half width equals the half length (x = y). For a rectangular basin, if the user wants the water-table changes perpendicular to the long side, specify x as the short dimension and y as the long dimension. Conversely, if the user wants the values perpendicular to the short side, specify y as the short dimension, x as the long dimension. All distances are from the center of the basin. Users can change the distances from the center of the basin at which water-table aquifer thickness are calculated.

Cells highlighted in yellow are values that can be changed by the user. Cells highlighted in red are output values based on user-specified inputs. The user MUST click the blue "Re-Calculate Now" button each time ANY of the user-specified inputs are changed otherwise necessary iterations to converge on the correct solution will not be done and values shown will be incorrect. Use consistent units for all input values (for example, feet and days)

	Input Values		use consistent units (e.g. feet & days or inches & hours)	Conversion Table	
				inch/hour feet/	day
	0.2300	R	Recharge (infiltration) rate (feet/day)	0.67	1.33
	0.200	Sy	Specific yield, Sy (dimensionless, between 0 and 1)		
Н	5.40	К	Horizontal hydraulic conductivity, Kh (feet/day)*	2.00	4.00 In the report accompanying this spreadsheet
	55.000	x	1/2 length of basin (x direction, in feet)		(USGS SIR 2010-5102), vertical soil permeability
	12.000	У	1/2 width of basin (y direction, in feet)	hours days	
	1.000	t	duration of infiltration period (days)	36	1.50 hydraulic conductivity (ft/d).
	25.000	hi(0)	initial thickness of saturated zone (feet)		

maximum thickness of saturated zone (beneath center of basin at end of infiltration period)

maximum groundwater mounding (beneath center of basin at end of infiltration period)

Ground-Distance from center of basin

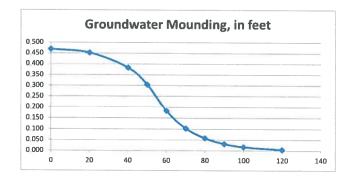
h(max)

Δh(max)

water Mounding, in in x direction, in



Re-Calculate Now



Disclaimer

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

APPENDIX - D

Stormwater Operation and Maintenance Plan and Long Term Pollution Prevention Plan

Standard 9

<u>Triangle</u>	<u>Farm</u>
Halliston	Massachusetts

Stormwater Management Operation and Maintenance Plan And Long Term Pollution Prevention Plan

Triangle Farm Holliston, Massachusetts

May 8, 2020

In accordance with Standard 9 of the Massachusetts Department of Environmental Protection Stormwater Handbook (February 2008), the attached on-site maintenance program for the proposed stormwater management system has been developed to ensure the Best Management Practices (BMP's) in place will remain functioning as designed. The Plan contains both construction period operations and maintenance as well as post construction responsibilities that shall "run" with the property if ownership is transferred.

Land Owner/Operator:

Thomas Murch Murch Prentice Realty Trust 5855 Lyman Road Turin, NY 13473

Date	

Estimated Maintenance Yearly Budget:

Annual Catch Basin and Oil/Grit Chamber Cleaning: \$ 600.00

Mowing, vegetation maintenance of Drainage Basins: \$ 300.00

Repairs: \$ 250.00

Total \$1,150.00

Holliston, Massachusetts

Construction Period Operation and Maintenance:

Good Housekeeping Practices:

- Remove all debris from site and dispose of in trash dumpsters
- Plan for adequate disposal of scrap, waste and surplus materials
- Keep work area clean
- Secure loose or light material that is stored on the site
- Store flammable materials apart from other materials
- Secure all materials at the end of each work day
- Maintain a clean neat and orderly site

Safety:

Keep safety considerations at the forefront of inspection procedures at all times. Likely hazards should be anticipated and avoided. Never enter a confined space (outlet structure, manhole, etc) without proper training or equipment. A confined space should never be entered without at least one additional person present. If a toxic or flammable substance is discovered, leave the immediate area and contact the local authorities at 911.

All cast iron storm water structure grates and covers shall be kept in good condition and kept closed at all times. Any damaged or broken structures will be replaced immediately upon discovery.

Erosion Control Barriers:

Compost filter socks shall be installed where indicated on the plans and in other appropriate locations where warranted. These barriers shall be installed prior to the commencement of any work on-site and in accordance with the construction plans. A supply of filter socks and compost filter material shall be kept on-site to replace and/or repair barriers that are damaged or degraded. The barriers shall be observed and maintained on a weekly basis during construction.

Construction Entrances:

The existing paved site entrance shall be utilized for construction access.

Catch Basin Protection:

Temporary inlet protection barriers consisting of Silt Sacks® will be placed within all constructed inlets to prevent inflow of sediments into the constructed drainage system. The barriers shall remain in place until a permanent cover is established or diversions away from the inlets are constructed. The barriers shall be observed and maintained as necessary on a weekly basis and after every rainfall of 0.5 inches or more.

Dust Control:

Soils information for the site indicates that it is comprised of sandy soils. Therefore, Dust control BMPs to reduce surface activities and air movement that causes dust to be generated from disturbed soil surfaces will be required. The preferred measure for dust control is sprinkling/irrigation. This is an on-going/as-needed requirement until surfaces have been stabilized. There shall be a water truck on-site available as needed.

GLM Engineering Consultants Inc.

Holliston, Massachusetts

Spill Control:

A contingency plan to address the spillage/release of petroleum products and any hazardous materials will be implemented for the site during construction. The plan will include the following measures:

- Equipment necessary to quickly attend to inadvertent spills or leaks shall be on-site in a secure but accessible location. Such equipment will include, but not be limited to, the following: urethane drain cover seals (mats), a spill containment kit which includes sand and shovels, suitable absorbent materials, storage containers, safety goggles, chemically resistant gloves and overshoe boots, water and chemical fire extinguishers, and first aid equipment.
- Spills or leaks will be treated properly according to material type, volume of spillage and location of spill. Mitigation will include preventing further spillage, containing any spilled material to the smallest practical area, removing spilled material in a safe and environmentally friendly manner, and remediating any damage to the environment.
- The contractor shall be familiar with the reporting requirements of the Massachusetts
 Contingency Plan (310 CMR 40.00) as issued by the Massachusetts Department of
 Environmental Protection (DEP); specifically Subpart C Notification of Releases and Threats
 of Release of Oil and Hazardous Materials and Subpart D Preliminary Response Activities and
 Risk Reduction Measures.
- For any large spills. The Massachusetts DEP Hazardous Waste Incident Response Group shall be notified immediately at 1-617-792-7653 and an emergency response contractor will be called in.

Holliston, Massachusetts

Post-Construction Period Operation and Maintenance:

Pavement Sweeping:

Sweeping has been shown to be an effective initial treatment for reducing contaminants in stormwater runoff. Sweeping is not required to meet TSS removal goals in this case but should be performed in the spring to remove winter accumulations or at other when warranted.

Gutter Cleaning:

Gutter cleaning shall be done at least once per year, in the fall after the trees have dropped their leaves. Inspect downspouts and overflows periodically to prevent debris buildup.

Deep Sump Catch Basins:

Deep sump catch basins remain effective at removing pollutants only if they are cleaned out frequently. Inspect and clean sumps when sediments whenever the depth of deposits is greater than or equal to one half the depth from the bottom of the invert to the lowest pipe in the basin, at least once (1) time per year, at the end of the foliage and snow removal seasons. Clamshell buckets or vacuum trucks shall be utilized.

Recharge Systems (Infiltration Chambers):

The inlet pipe and observation access port shall be inspected 4 times per year. Inspect recharge facilities following a rainfall event greater than 2.5 inches in a 24 hour period. Any accumulated debris shall be removed.

If standing water is observed for more than 72 hours following a storm event, immediately retain a qualified professional to assess whether infiltration function has been lost and develop recommended correction actions.

If upon visual inspection it is found that sediment has accumulated, a stadia rod should be inserted to determine the depth of sediment. When the average depth of sediment exceeds 3 inches throughout the length of the chambers, clean-out should be performed. Maintenance is accomplished with the JetVac process. The JetVac process utilizes a high pressure water nozzle to propel itself down the Isolator Row while scouring and suspending sediments. As the nozzle is retrieved, the captured pollutants are flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/JetVac combination vehicles.

Drainage Basin & Forebay:

Vehicle access if necessary will be via the 10 foot wide access around the top of the retention basin. The drainage easement shall be mowed twice a year and kept clear of any trees. The easement will be used for access to the basin.

Inspect it after every major storm for the first few months to ensure it is stabilized and functioning properly and if necessary to take corrective action. Also inspect the basin every time there is a discharge through the high outlet weir. A major storm is defined as a storm that is equal to or greater than the 2.5 inches in a 24-hour storm. Note how long the water remains standing after a

Triangle Farm

Holliston, Massachusetts

storm. If longer than 72 hours, there may be clogging of the infiltrative surfaces. Inspect the basin and mow it as needed. When mowing keep the grass height no greater than 6 inches. Set mower blades no lower than 3 to 4 inches. Remove grass clippings, organic matter and trash. Use deep tilling to break up compacted or clogged surfaces.

Check for signs of gullying and repair as needed. After removing the sediment, replace any vegetation damaged during the clean-out by reseeding.

Outlet Structure:

Inspection: Inspect semi-annually the first year, and at least once a year thereafter. Inspect the grass for growth and the side slopes for signs of erosion and formation of rills and gullies. Plant an alternative grass species if the original grass cover is not successfully established.

The stone riprap outlet channel shall be inspected semi-annually for debri, sediment buildup and any vegetated growth.

Sediment Removal: Check on a yearly basis and clean as needed. Use hand methods (i.e., a person with a shovel) when cleaning to minimize disturbance to vegetation and underlying soils.

Snow Removal and De-icing:

The use of Sodium Chloride ("rock salt") for de-icing of paved surfaces will be limited; except when found to be necessary for safety of the workers. Sand will be the primary icing control agent. Alternative de-icing products such as calcium chloride may be used as temperatures or other conditions warrant.

Fertilizer:

Slow release organic fertilizers will be used in landscape areas to limit nutrient transport to groundwater and wetland areas. Application will be limited to 3 lbs. per 1000 sf of lawn area.

Spill Control:

See Construction Period Spill control requirements.

Triangle Farm			
Holliston, Massachusetts			

Stormwater Construction Site Inspection Report

Stormwater Construction Site inspection Report					
General Information					
Project Name	Triangle Farm				
MA DEP File No.		Location			
Date of Inspection		Start/End Time			
Inspector's Name(s)					
Inspector's Title(s)					
Inspector's Contact Information					
Inspector's Qualifications					
Describe present phase of construction					
COMME MEMORIA					
Type of Inspection:					
☐ Regular ☐ Pre-storm event	☐ During storm event	☐ Post-storm event			
	Weather Inf	ormation			
Has there been a storm event since	the last inspection? \(\sigma\)Ye	s □No			
If yes, provide:	T (1)				
Storm Start Date & Time: St	torm Duration (hrs):	Approximate Amount of Precipitation (in):			
Weather at time of this inspection?					
•	☐ Sleet ☐ Fog ☐ Sne	owing High Winds			
Other:	Temperature:				
Have any discharges occurred since the last inspection? □Yes □No					
If yes, describe:					
Are there any discharges at the tim If yes, describe:	e of inspection? □Yes □	lNo			

Site-specific BMPs

- Number the structural and non-structural BMPs identified in your SWPPP on your site map and list them below (add as many BMPs as necessary). Carry a copy of the numbered site map with you during your inspections. This list will ensure that you are inspecting all required BMPs at your site.
- Describe corrective actions initiated, date completed, and note the person that completed the work in the Corrective Action Log.

	BMP	BMP Installed?	BMP Maintenance Required?	Corrective Action Needed and Notes
1		□Yes □No	☐Yes ☐No	
2		□Yes □No	☐Yes ☐No	
3		☐Yes ☐No	☐Yes ☐No	
4		☐Yes ☐No	☐Yes ☐No	
5		□Yes □No	☐Yes ☐No	
6		□Yes □No	☐Yes ☐No	
7		☐Yes ☐No	□Yes □No	
8		□Yes □No	☐Yes ☐No	
9		□Yes □No	☐Yes ☐No	

	Triangle Farm Holliston, Massachusett	is .			
	ВМР	BMP Installed?	BMP Maintenance Required?	Corrective Action Needed and Notes	
10		□Yes □No	☐Yes ☐No		

	Non-Compliance
cribe any incidents of non-compliance	e not described above:
	CERTIFICATION STATEMENT
accordance with a system designed submitted. Based on my inquiry of t for gathering the information, the in	his document and all attachments were prepared under my direction or supervision to assure that qualified personnel properly gathered and evaluated the information he person or persons who manage the system, or those persons directly responsible formation submitted is, to the best of my knowledge and belief, true, accurate, and significant penalties for submitting false information, including the possibility of finations."
Print name and title	

<u>APPENDIX – E</u>

Illicit Discharge Statement

Standard 10

Triangle Farm	
Holliston, Massachusetts	
Illicit Discharge Compliance Statement	
Triangle Farm Holliston, Massachusetts	
May 8, 2020	
This statement is provided in accordance with the provisions of the Massachu Stormwater Management Standard #10.	ısetts
To the best of the applicant's/owners knowledge there are no illicit discharge site's stormwater manangement system.	s to the
All proposed uses on the site will not generate, store or discharge any polluta groundwater and/or wetland resource areas.	nts to the
Any illicit discharges identified during or after construction will be terminated immediately.	l
Applicant/Owner:	
Thomas Murch, Trustee	

Date

Murch Prentice Realty Trust

2855 Lyman Road Turin, NY 13743

Signature

<u>APPENDIX – F</u>

Soil Evaluation Forms

Location Address or Louisia. Lot Z MILLS. Hourston

On-site Review

Deep Hole Number 2A Date: 5/17	/97 Time: AN	Weather 56 Du
Location (identify on site plan)		
	s, <5 Surface Stones	Ns
Vegetation HIGH GPASS		
Landierm TERRACE		
Position on landscape (sketch on the back)		
Distances from:		
Open Wate: Body Teat	Orainage way 7 fee	as b of t
Possible Wet Arez 140 + feet	Property Line fee	• •
Drinking Water Well 7 feat	J:ner	

DEEP OBSERVATION HOLE LOG								
Depth from Surface nones,	Sou Honzor,	Sc:Texture (USDA	CITIEXTURE SCIEGOR So Other (USDA (Munae Motting IStructure Stones Boulders, Consistency, Fa					
9	A _P	Lagra	1042 3/3					
25''	3~	Serricy L-2101 10485/6						
42"	С,		2.5 4 5/2		30% Genvel			
6E"	C ¿		2.5 7 5/4	68"	CCARSE 70% GRAVEL			
124" C3 2.5 45/2 30; GREVE!								

William A O. F. Defice with Street and the street	JULI JUNIANIA
Parent Material (geologis) TILL	Depth to Bodrook N/A
Gasthiss Graundwater: Standing Water In the HUG	Westingfrom Fiface 68"
Estimated Seasonal High Ground Water 68"	



DEP APPROVED FURY - 12 7 17

Location Address or Lot No. Lot 2 MILL ST House soul

Orinking Water Well To feet

Deep Hole Number ZB Dar	e: 5/12/97	Time: Ar(17/65:-3:	25. 700
Location (identify on site plan)	•			
Land Use OPEN FIELD	Sippe (%) <.	Surface Stones	, No	
Vegetation 4/6H 6FADS				
Landform . TERRACE				
Position on landscape (sketch on t	he back)			
Distances from:				
Open Wate: Body =	feet Drai	tage way fill fe	est	
Possible Wet Area 140+	feet Prop	erty Line fe	2 1	

DEEP OBSERVATION HOLE LOG								
Cesth from Surface (Inches)	Seil Herizen	Sc Texter (JSDA)	So. Co si Milynag		Other (Structure, States Boulders, Consistency, % Grave.			
12"	A.P	Lance	10423/3					
26"	Bw	Series	10425/L					
				e 46"				
130'	C	SANDY	2.5 y 5/2		ZC% GEAVEL			

• អា អាធាចមា ០៖	2 house Redukted At a	JEH! PROPUSED DISH	JSA.ARIA		
Parent Material (geologia	TILL	The state of the s	OesthiaBearask	NA	and the same of th
Danih to Groundwater	Standing Water In the Full	the sales of the same of the sales of the sales and the sales of the s	Wagn of from he had	104"	
Estimated Seasonal High	Ground Water	46"			



Location Address or Lot No. Lot Z Mile St. Holliston

DEEP OBSERVATION HOLE LOG								
Depth from Surface (Inches)	Sail Harizañ	Sc!Texture (JSDA	Spal Cale: (Munsell)	So Marting	Other (Structure, Stones, Boulders, Consistency, %: Gravel.			
10	A.	Laries	104E 3/3					
32"	Dw	Serior	1048 5/6	C 32'				
					7			
120"	۲,	SANCY	2.545/2					

111111111111111111111111111111111111111	A TIGATO INT TOWNER WILL COMMITTE	tie data a fri data cured	
Parent Material Igeologic	TILL		. D/n
Dagin to Groundwater.	Standing Water in the Hold		For Fiface
Estimated Seecond High	Ground Water 32"	Pallatin tikkaningan silip salippa <u>n saga saga saga saga</u> ngan kanangan sagan	



Location Address or Lot No. LOT Z Mill STREET HOLLISTEN

COMMONWEALTH OF MASSACHUSETTS

, Massachusetts

	Percolation	Test*
Date:	5/12/97	Time:
Observation Hole #	l	OVERNIGHT 2
Depth of Perc	46"	50"
Start Pre-soak	11:17	F:13
End Pre-soak	11:32	8:28
Time at 12"	11:32	8: 28
Time at 9"	11:55	9:01
Time at 6"	12:25	10:00
Time (9"-6")		
Rate Min./Inch	10:0	. 20.0

^{*} Minimum of 1 percolation test must be performed in both the primary area AND reserve area.

Site Passed	Site Failed			
Performed By:	JOSEPH	NIHILL		 * • • • • • • • • • • • • • • • • • • •
Witnessed By:			ST :	18
Comments:				11



Location Address or Lot No. Lot 18 MILL ST. HOLLISTON

Deep Hole Number 18A	Date: 10/20/98	Time: AM	Weather	50 JUN
Location (identify on site plan)				
Land Use OPEN FIELD	Slope (%)	<5 Surface Stones	20	
Vegetation HIGH GRASS				
Landform TERRACE				
Position on landscape (sketch	on the back)			
Distances from:				
Open Water Body -	feet	Drainage way fee	t	
Possible Wet Area 12	20+ feet	Property Line fee	•	
Drinking Water Well	feet	Other		

		DEEP OB	SERVAT	TION HOI	_E LOG'
Depth from Surface (Inches)	Soil Horizon	Soil Texture (USDA)	Soit Color (Mansell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
8"	A.	Loan	10483/2		
24"	Bw	Sanoy	10425/6		
				≥24"	
					20% GRAVEL
					COBBLES /STONES
		SANOY			
120"	C JM OF 2 HOLES I	Loan	2.545/3		

Parent Material (geologic	Tici		DepthtaBedrock:	N/A	
Depth to Groundwater:	Standing Water in the Hole:	NONE	Weeping from	Pit Face: 10	00"
Estimated Seasonal High	Ground Water	24"			



Location	Address	or	Loi	No.	LOT	18	Mill	St.	HOLUSTON

Deep Hole Number 183	Date: 10/20/48	Time: AM	Weather	20, JUN
Location (identify on site plan) Land Use OPEN FIELD	Slope (%)	<5 Surface Stone	es No	
Vegetation HIGH GRASS				
Landform TERRACE				
Position on landscape (sketch	on the back)			
Distances from:				
Open Water Body	feet	Drainage way	feet	
Possible Wet Area	lo+ feet	Property Line	feet	
Drinking Water Well	- feet	Other		

		DEEP OB	SERVAT	ION HOI	LE LOG'
Depth from Surface (Inches)	Soil Harizon	Soil Texture (USDA)	Soil Calar (Munseli)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
10"	A?	LOAM	10423/2		
24"	Bw	Sanoy	104R 5/C		
				228	
				Stramation of the state of the	~.
					15% GRNEL
		0			
122"	C	SAROY	2.5 ₄ 5/3		

* MINIMUM OF	2 HOLES REQUIRED AT EVI	ERY PROPOSED DIS	POSAL AREA		
Parent Material (geologic)	TILL		DepthtoBedrock	N/n	
Depth to Groundwater	Standing Water in the Hole	00	Weeping from F	Pit Face: 70"	
Estimated Seasonal High	Ground Water: 28	bs			-



Location Address or Lot No. Lot 18 MILL ST. HOLLISTON

COMMONWEALTH OF MASSACHUSETTS

. , Massachusetts

	Percolation T	est*
Date: 14	0/21/98	Time:
Observation Hole #	1	Z
Depth of Perc	42"	42"
Start Pre-soak (OVERNIGHTS)	8:26	8:28
End Pre-soak	8:41	8:43
Time at 12"	8:41	8:43
Time at 9"	9:32	9:05
Time at 6"	11:02	9:34
Time (9"-6")	90 mis.	29 MIN.
Rate Min./Inch	30 .	10

Minimum of 1 percolation test must be performed in both the primary area AND reserve area.

Site Passed	Site Failed]	W.		
		***************************************			****
Performed By: _	JOSEPH	NIHILL	•	= 3)	
Witnessed By: _	NICOLE	LETENDRE			
Comments:					



Location Address or Lot No. LOT 17 MILL ST. HOLLISTON

On-site Review

Deep Hole Number 17 A	Date: 10/20/98	Time: A M	Weather 50° Sull
Location (identify on site plan) Land Use OPEN FIELD	Slope (%)	<5 Surface Stones	NO
Vegetation HIGH GRASS			*
Position on landscape (sketch	on the back)		
Distances from: Open Water Body Possible Wet Area Drinking Water Well	feet 20+ feet — feet	Drainage way fe Property Line fee Other	

		DEEP OB	SERVAT	ION HO!	LE LOG°
Depth from Surface (Inches)	Soil Harizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
12"	Ao	Loam	10yR 3/2		
. 24	B	Sanoy	loye5/6	ಎ20°	
					15% GRAVEL
					COBBLES /STONES
126"		SANDY	2.5,5/3		



Location Address or Lot No. Lot 17 MILL St. HOLLISTON

Deep Hole Number 17B	Date: 10/20/98	Time: A M	Weat	her 50° Sun
Location (identify on site plan) Land Use OPEN FIELD Vegetation HIGH GRASS		∠S Surface S	tones NO	
Landform TERRACE				
Position on landscape (sketch o	n the back)			
Distances from:				
Open Water Body —	feet	Drainage way	feet	
Possible Wet Area 120	+ feet	Property Line	fee:	
Drinking Water Well -	feet	Other		

		DEEP OB	SERVAT	ION HOL	LE LOG°
Depth from Surface (Inches)	Soil Horizon	Spil Texture (USDA)	Soil Caler (Munsell)	Soii Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
6"	Ap	Loan	104R3/2		
24"	B	Samoy	104R5/L	۵22"	
34"	C.	SILTY	104R4/4		
120''	Cz	Sanoy	2.5× ^{5/4}		20% GRADEL COTBLED/STONES

TATILATIO OF CT	2 7.0000		
Parent Material (geologic	TILL	DepthtoBedrock: 0/	A
Depth to Groundwater	Standing Water in the Hole 72"	Weeping from Pit Face:	72"
Estimated Seasonal High	Ground Water: 22"		



Location Address or LOI NO. LOT 16 MILL ST. HOLLISTON

Deep Hole Number 16A	Date: 10/20/98	Time: AM	Weather 50° Sun
Location (identify on site plan) Land Use OPEN FIELD	Slope (%)	<5 Surface Stone	es NO
Vegetation HIGH GRASS	>		
Landform TERRACE			
Position on landscape (sketch	on the back)		
Distances from:			
Open Water Body	feet	Drainage way	feet
1 033.510	oo */ feet		feet
Drinking Water Well	- feet	Other	

DEEP OBSERVATION HOLE LOG						
Depth from Surface (Inches)	Soil Horizon	Spil Texture (USDA)	Spil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)	
8"	Ap	LOAM	104R 3/2			
. 24"	Bu	Sanoy	loye5/6	216")*	
					10% GRAVEL COBBLES / BLDRS	
					COBBLES / BLDRS	
		SANDY	۵			
126"	C		2.5,5/3	Markata Ale		

. MINIMUM OF	· 5 HOFF2 MEGRIMED WILE.	VERT PROPUSED DISPO.	JALANICA .		
Parent Material (geologic	Tice		DepthtoBedrock:	N/A	
	Standing Water in the Hole		Weeping from Pit I	Face:	92"
Setimated Seasonal High	4 . 46				



Location Address or Lot No. Lot 16 MILL St. HOLLISTON On-site Review

Deep Hole Number 16B Date	e: 10/20/98	Time: A M	Weather 50° Sun
Location (identify on site plan) Land Use OPEN FIELD Vegetation HIGH GRASS Landform TERRACE	Slope (%)	<5 Surface Stones	70
Position on landscape (sketch on t	he back)		
Distances from:			
Open Water Body	feet	Drainage way - fee	et .
Possible Wet Area 100+/	feet	Property Line fee	t 🚎
Orinking Water Well	feet	Other	

DEEP OBSERVATION HOLE LOG'						
Depth from Surface (Inches)	Soil Herizan	Soil Texture (USDA)	Soil Color (Munsel)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, 54 Gravel)	
12°	A _e	Loam	104R3/2			
, 28°	Bu	Sanoy	loye5/6	22,		
					20% GRAVEL	
					COBBLES/STONES	
132"	C	Sanoy	2.5,5/3			

* MINIMUM OF	- 5 HOFER MEMORMED WE EAR	AT PROPOSED DISTOSALE				
Parent Material (geologic	Till	Depti	htoBedrock:	N/A		_
	Standing Water in the Hole	108"	Weeping from P	it Face:	72"	_
Estimated Seasonal High	Ground Water: ZZ"					



Location Address or Lot No. Lot 15 MILL ST HOLLISTON

On-site Review

Deep Hole Number 15A Date: 10	120/98 Time:	AM	Weather	50° Sun
	pe (%) < 5 Surfa	ace Stones	70	
Vegetation HIGH GEASS				
Landform TERRACE				
Position on landscape (sketch on the ba	ick)			
Distances from:				
Open Water Body - feet	Drainage way	- feet		
Possible Wet Area 130 + feet	t Property Line	feet		
Drinking Water Well - fe	et Other			

		DEEP OB	SERVAT	TION HO	LE LOG°
Depth from Surface (Inches)	Soil Harizon	Soil Texture (USDA)	Soil Color (Munsell)	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, % Gravel)
12."	Ap	Loan	10483/2		
28"	Bw	Sanoy	104R5/L	20"	11
5°.	C.	SILTY	10ye 4/4		COBBLES / BLDRS
			*		25% GRAVEL
		Sanor			COBBLES/BLDRS
122"	Cz	Sanoy	2.5,5/4		

MINIMUM OF 2 HOLES REQUIRED AT EVERY PROPOSED DIS	POSAL AREA
Parent Material (geologic)	DepthtoBedrock:
1 - 1	Weeping from Pit Face: 7Z "
Deptinte disposewater. Standing Water in the 110	Weeping nominates 1
Estimated Seasonal High Ground Water: 20	



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Location Address or Lot No. Lot 15 MILL ST. HOLLISTON

Deep Hole Number 158	Date!0/20/98	Time: 1M	Weather	50° JUN
Location (identify on site plan)				
Land Use OPEN FIELD	Slope (%)	<5 Surface Stones	20	
Vegetation HIGH GRASS				
Landform TERRACE				
Position on landscape (sketch	on the back)			
Distances from:				
Open Water Body		Drainage way - fee	:1	
Possible Wet Area 13	O+ feet	Property Line fee	i .	
Drinking Water Well	- feet	Other		

		DEEP OB	SERVAT	ION HO	LE LOG'
Depth from Surface (Inches)	Soil Horizon	Soil Texture (USDA)	Soil Calor (Munselli	Soil Mottling	Other (Structure, Stones, Boulders, Consistency, 5a Gravel)
10"	Ap	Loan	104R3/2		
24"	Bw	SAMOY	10425/6	220"	
52"	C.	SILTY	104R 4/4		
					150/
					15% GRAVEL
		SANDY	2/		COBBLES/BLDRS
124"	Cz	Loan	2.5 y 5/4		

* MINIMUM OF	2 HOLES REQUIRED AT EVER	TY PROPOSED DISPO	SAL AREA			
Parent Material (geologic)	TILL		DepthtoBedrock*	AIG		
	Standing Water in the Hole:	96"	Weeping from	Pit Face:	60"	
Estimated Seasonal High	Ground Water: 20"					



Location Address or Lot No. LOT 15 MILL ST. HOLLISTEN (RETEST)

Deep Hole Number Date: 5	23(0) Time AN	Weather 50' July
Location (identify on site plan		
	se (%) <5 Surface Stones	1/2
Vagatation 416H GANS		
Landform TERRACE		
Position on landscape (sketch on the bac	k)	
Distances from:		
Open Water Body To feet	Dramage way =fe	5∜
Possible Wet Area 140+ feet	Property Line fee	• •
Drinking Water Weil To fee	: Other	

		DEEP OB	SERVAT	ION HO	LE LOG'
Destin from Surface triches	Scil Hanzan	Schitexture (JSDA	Seli Celer (Munae	Notifus Notifus	Other (Structurs, Stones, Bouldars, Consistence, As Grave)
12	A, P	Lance	104c 3/2		
24'	BN	Samoy	1042 5/6		
				C 24"	
					87
					MED-FINE
120	C	SANDY	2.5 y 5/3	No. of the state o	10% Cabbles Cab/ Stones

101 10 10 10 10	ta notes had had not to the odes of so	2020-1-0		
Parent Materia I geologic	TILL	DepthtoBr	1.311	D/n
Diethia Grandwatar	Standing Visiter in the near Including	V. 60	2 mg [graft file]	100'
Estmate: Seasinal High	Ground Wilson 24 4			



Location Address or Lot No. Lot 15 MILLST. HOLLISTON (RE-TEST)

Deep Hole Number Z	Date: 5 23 0	Time: Art	VVestes	50. Jun
Location (identify on site plan)				
Land Use OPEN FIELD	Slope (%	; <5 Surface Stone	s No	
Vagetation HIGH GFASS				
Landform TERRACE .				
Position on landscape (sketch o	on the back)			
Distances from:				
Open Water Body -	feet	Drainage way	feet	
Possible Wet Area 140	C+ feet	Property Line f	201	
Drinking Water Weil	- fee:	Other		

DEEP OBSERVATION HOLE LOG							
Depth from Surface (Inches)	Sell Herizen	Sc.ii Texture (USDA;	Sal Color (Munsel)	50 Mottling	Other (Structure Stones Boulders Consistancy, Re Grave		
10	AP	Lance	104£ 3/2.				
Z4"	3~	Sanoy	104R 5/6				
				e 24"			
Table 1 and		SANDY			MED-FINE 10% GEAVEL		
120"	C	Lam	2.575/3		CLB/STONES		

HI HIND A C	. 5 UPTES UERRINED WITE	ME AN LUID LAGED DISUNG	m = = = =	
Parent Marena (geologic	TILL	Dept.	easaffad as f	NA
Digith to Groundwater	Standing Water in the Hold		Weeping from Fir Fa:	112"
Estimated Seattinal High	Ground Water	24"		



Location Address or Lot No. Let 15 Mill ST Halliston

COMMONWEALTH OF MASSACHUSETTS

. , Massachusetts

	Percolation Test	
Date:	5/23/01 Tim	ne:
Observation Hole #	1	Z
Depth of Perc	36"-54"	32 /50"
Start Pre-soak	7:55	7:52
End Pre-soak	2:10	8:07
Time at 12"	8:10	8:07
Time at 9"	2:50	9:01
Time at 6"	10:00	10:25
Time (9"-6")		
Rate Min./Inch	24:0	28.0

^{*} Minimum of 1 percolation test must be performed in both the primary area AND reserve area.

Site Passed	Site Failed			
		to the collegement of the college of		
Performed By:	JOSEPH	NIHILL		8
Witnessed By:				
Comments:	anaphilipating stratistischen 4 diplikkrikationischen assisteren s		dimensional systematorian di sponsonomia	and the state of t



Location Address of Lot No Lot 4 Mile St. Hourston

Deep Hole Number 4A Date: 5/12/	97 Time, AM Weather 50' Su
Location (identify on site plan)	
	<5 Surface Stones No
Vegetation HIGH CANS	
Landform TERRACE	
Position on landscape (sketch on the back)	
Distances from:	
Open Wate: Body To feet	Dramage way feet
Poscible Wet Area 140+ feet	Property Line feet
Drinking Water We'l feet	Other

DEEP OBSERVATION HOLE LOG						
Depth from Surface Inchesi	Souther zen	Sch Texture	So Co or	Sc North	Othe: (Structure, Stoned Bouldard, Consistancy, 1a Grave)	
10"	AP	Lance	10423/2			
24"	B~	Samoy	1048 5/6			
				@ Z4"		
A contraction of the contraction					Zo %. GRAVEL	
120"	C	SANDY	25 y 5/3		w/ Cobbles	

' MAMAN U	. 5 unita utinitan yi avada butinitan san na	rubal Ahsa	
Parent Materia (geologia	TILL	DepthipBedrask	D/A
<u> Denthita Groundwater</u>	Standing Water to the Help	Wessing the Picasa	28"
Estimated Seasonal High	Ground Warerl		



Location Address or Lot No Lot 4 Mile St. Hourston

Deep Ho	e Number	43	Date	: 5/12/9	7	Time:	1.12(Wester	56.	Sun
Location	(identify on	site plan	}	, ,							
	OPEN F			Slope (%	, <5	Surfa	ice Ston	ies M	Ü		
	a Hiller		•								
Landform	122	RALE									
Position (on landscap	e (sketch	on th	e back)							
Distances	from:										
C	pan Water	Body -	-	tee:	Drainag	e way	gar.	feet			
P	ossible Wet	Ares 14	10+	feet	Propert	y Line		feet			
D	rinking Wat	er Well	-	feet	Otner						

DEEP OBSERVATION HOLE LOG'						
Depth from Surface (Inches)	Sall Horzan	Scillexture (USDA)	Soli Color (Munse)	Son Montag	Other (Structure, Stones, Boulders, Consistency, Na Grave	
10"	AF	1-203100	104c 3/3			
24''	Bw	Sanoy	10YR 5/6			
			The state of the s	024"		
					Zo / GRAVEZ	
		SUNDA			w/ (cbble>	
132''	C	Lo.7m	2.545/2			

MANAGAN OF 2 HOUSE HEQUITED AT EVERY PASHUS	IJ SaUSALARSA
Parent Material (geologis)	DepthoRedrose D/n
Charthire Graundwater. Standing Water in the Hala	Weeding Fig. Face 32 "
Estimated Seasonal High Ground Water 29	<i>'</i>



feet

Location Address or Lot No. LET 4 MILLST. HOLLISTON

Possible Wet Area 140 + feet Property Line

Drinking Water Weil 7 feet Other

HSE HOLE			<
Deep Hole Number 4C Date: 5/12/97	Time: AA(11.65. 5.	25. JAN
Location (identify on site plan)			
	<5 Surface Stones	No	
Vegetation HIGH GFASS			
Landform TERRACE			
Position on landscape (sketch on the back)			
Distances from:			
Open Wate: Body To feet 5	Drainage way - fee	*	

	DEEP OBSERVATION HOLE LOG'					
Deptin from Surface (Inches)	Soil Horzon	Soli Texture (USDA)	Sell Color (1/10/13:20)	Soi Mariles	Other (Structure: Stones Boulders Consistency, Re Grave	
10	AP	Long	1042 3/3			
20"	3∾	Sanoy	104R5/C			
			And the second s	C 24"		
		Section of the sectio				
			All the state of t			
126"	C	LOMM	2.545/2	-		

111 4 414 41 104	- 11G-13 11G-17 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	
Parent Materia (geologic	TICL	DepthtoBodrass
Deern op Orn Edwaran	Standing Water intrah. 3	Weed to from Pit Face 24 "
Est marzo Sasconal High	Ground Water	



Location Address or Lot No. LET 4 Mill ST Hellister

COMMONWEALTH OF MASSACHUSETTS

, Massachusetts

Percolation Test*						
Date:	9/10/97 Time	e: .				
Observation Hole #	OVERNICHT !	OVERNICUT Z				
Depth of Perc	44 "	40"				
Start Pre-soak	2:67 8:07	8:10				
End Pre-soak	8:22	8: 26				
Time at 12"	8:22	8:26				
Time at 9"	9:05	2:57				
Time at 6"	10:14	9:50				
Time (9"-6")						
Rate Min./Inch	25.0.	18.0				

* Minimum of 1	percolation t	est	must	be	performed in	both	the primary	area	AND
reserve area.			•						

Site Passed	Site Failed		ø	-
Performed By:	JOSEPH N	1 Hech		T TESSEMBLE CONTRACTOR OF THE STANSON OF
Witnessed By:				
Comments:		entermonente anadolimente entermone en la distanción solar entermonente	A CONTRACTOR OF THE PARTY OF TH	Named and American States



Michaellan Address or Lot No. Lot 3 Mich St. Howaston

Deep Hole Number 3A Date: 51	12(9) Time AN	Weather 52 Suu
Location (identify on site plan)		
	e (35) <5 Surface Stones	No
Vegetation HIGH GEASS		
Landform TERRACE		
Position on landscape (sketch on the back	<i>(</i>)	
Distances from:		
Open V/ate: Body T fee:	Drainage way in fe	: T.*
Possible Wet Area 140 + feet	Property Line fe	¢ 4
Crinting Mater Well To feet	Dinar	

	DEEP OBSERVATION HOLE LOG					
Depth from Surface Inchesi	Self Herizen	Sc.l Texture (USDA	So Color (IV) -52	Sc test	Other (Structure, Stones, Boulders, Consistency, %) Grave	
12"	AP	Lance	10463/3			
26"	BN	Senoy	10YR5/6			
			r manufacturing de la lac	032"		
			- And the order of the contract of the contrac			
					POCKETS OF CEARSE GRAVEL	
134"	C	SAUDY	2.5 y 5/2			

البيا المالي ويروزه = الموا	Lit Herea Willer with William	0010000	7-71-7		
Parent Material (geologia			Desthis Destrock	D/n	
Darrich de Groundwater	Standing Water in the #23		Weep na 15- 2-1	310 96"	
Est mated Seasonal High	Ground Warell	32 "			



Location Address or Lot No. Let 3 MILLST HOLLISTEN

Drinking Water Well To feet

On-site Review

Deep Hole Number 35	Date: 5/12/97	Time: Ar(Westra	20. 700
Location (identify on site plan)				
Land Use OPEN FIELD	Slope (34) <2	Surface Stones	No	
Vegetation HIGH GFASS				
Landiorm TERRACE				
Position on landscape (sketch	on the back)			
Distances from:				
Open Water Body	feet Drain	lage way - fea	6. b	
Possible Wet Area 14	Of feet Prop	erty Line fee	a 	

Oine:

		DEEP OB	SERVAT	TION HOI	LE LOG
Debtif from Surface Inches)	Seil Herizon	Scil Texture IUSDA:	Sp. Color (Munae	So Mot. ng	Other (Structurs: Stones, Boulderd, Consistend V, %) Grave
10 '	AP	Lance	1042.3/3		
24"	3~	Sanoy	10YR 5/6		
				C 32"	
					,
			Transfer or the state of the st		
128''		SANDY	2.5 y S/3		Pockets of FINE SAND

		0 0 1 1 2 7 1 1 2 1	
Parent Morena ligeologic	TILL	Depthio BestockA)/n
There is Cont. Indicator	Standing Water in the Hole	Wessing from P. Fire	64"
Est marad Seasona High	Ground Waren 32 "		



Location Address or Lot No. LET 3 MILL St. Holliston

On-site Review

<_
25. 201

		DEEP OB	SERVAT	ION HO	LE LOG'
Deptin from Surface inches)	Soil Horizon	Soil Texture (USDA)	Soll Color (Menser	So Motting	Other (Structure Stance, Boulders Consistency, Re Grave
12 4	人。	Lonix	1045 3/3		
36"	Bn	Semoy	1048.5/L		
The state of the s			Andrews on the Control of the Contro	0 28 +	
			II III. Saarii Peranayani are david		-
The second of th					
132"	C .	SMOY	2.5 y 5/z	NA WATER-WATER T-M- CARD-T- T-M-	



DEP APPROVED FORM 12 12 12

Location Address or Lot No. Lot 3 M. 11 ST Holliston

COMMONWEALTH OF MASSACHUSETTS

, Massachusetts

Percolation Test*							
Date:		Time:					
Observation Hole #		2					
Depth of Perc	44"	44"					
Start Pre-soak	12:55	1:52					
End Pre-soak	1:11	2:67					
Time at 12"	1:11	2:07					
Time at 9"	1:18	2.26					
Time at 6"	1:58	2:54					
Time (9"-6")							
Rate Min./Inch	4.0	. 10.0					

reserve area.	percolation	test	must be	performed	in both	the	primary	area	AND
1000.70 8168.		*							

Site Passed	Site Failed				
Performed By:	JOSEPH		d tale mental edes sengen engages of the head to be set as a second	a S Δ is a substantial traps p the S P . Since S Δ are some	TO Salimphystococcus FT 5.55 (for max.) a v v
Witnessed By:					
Comments:	relaktivistel ste attitutastikkeleitiin erintestatutusentistel attivisentättistelei kev	and the second contraction of the second con	B. I	No. A. To and description of the Company of the Com	



APPENDIX – G

Supplemental Stormwater Plans

Pre-Development Subcatchment Areas
Post-Development Subcatchment Areas
Hydraulic Subcatchment Areas

